Summary of ICCR Source Work Group Meeting October 30, 1997 Internal Combustion Engines Work Group Meeting

I. Purpose

The main objectives of the meeting were to obtain consensus on the Test Plan, the Preliminary MACT Floor, and the presentations on the Test Plan and Preliminary MACT Floor, and to identify new tasks which need to be addressed by the Work Group (WG).

II. Location and Date

The meeting was organized by the Environmental Protection Agency (EPA) and was held at the Skybird Meeting Center at O'Hare Airport in Chicago, Illinois. The meeting took place on October 30, 1997.

III. Attendees

Meeting attendees included representatives of the OAQPS Emission Standards Division, trade associations, universities, and state agencies. A complete list of attendees, with their affiliations, is included as Attachment I.

IV. Summary of Meeting

The meeting consisted of discussions between WG members on selected issues which are listed below. The order of the meeting followed the agenda provided in Attachment II. A bullet point summary of the meeting is presented as Attachment III.

The topics of discussion included the following:

- Emissions Subgroup Report on Changes to Test Plan
- Dry Run of Test Plan Presentation and Discussion
- Population Subgroup Report on Changes to Preliminary MACT Floor
- Dry Run of Preliminary MACT Floor Presentation and Discussion
- Economics WG Presentation on Inter-Work Group Coordination
- Model Plants Development
- Next Meeting Issues

Emissions Subgroup Report on Changes to Test Plan

Sam Clowney presented a report on the RICE Test Plan drafted by the Emissions Subgroup. A copy of the Test Plan under discussion, which was sent out prior to the meeting, is included as Attachment IV.

Brahim Richani raised the issue of the inclusion of a justification for excluding dioxin from the HAPs list of the Test Plan. It was brought to a consensus that a brief justification be made in the test plan regarding dioxin being omitted from the pollutant list. It would address the concern with two points: 1) in the Dioxin Primer, IC engines were given a very low to moderate rating for possible emissions of dioxin, and 2) no chlorinated hydrocarbons are emitted, from natural gas or dieselfired engines therefore no dioxin can be formed.

It was agreed that once this revision is made, the Test Plan will be complete and ready to be presented to the CC.

Dry Run of Test Plan Presentation and Discussion

Sam Clowney presented the draft Test Plan Presentation to the WG. This presentation is included as Attachment V.

The topics of discussion which followed included moving ahead with the developed test plan, selection of possible test sites, and addressing the CC.

Moving Ahead with the Developed Test Plan

Ed Torres suggested that the RICE WG could move faster through the testing process by obtaining the budgeted amount of money (\$610K) from EPA, and contracting the testing out instead of letting the TMPWG take charge. Amanda Agnew questioned the forward motion without the oversight of EPA. Bryan Willson stated that this might be risky, since there is still no environmental representation on the RICE WG. Amanda Agnew said she would consult Terry Harrison on this issue further and report back to the RICE WG.

Selection of Possible Test Sites

The next step in the testing process is the selection of possible test sites for engine testing. Several test sites have been suggested by Sam Clowney, and PRC International and AGA are now looking at these sites for approval. The final determination

on the availability of these sites will be known by the end of November.

Don Price will look into possible test sites in California which have four stroke spark ignition engines with NSCR.

Bob Stachowicz suggested that catalyst manufacturers be contacted to determine if they would be willing to support the ICCR effort by donating or providing a reduced cost for catalysts for engine testing.

It was also suggested that engine testing be performed at the Engine and Energy Conversion Research Lab (EECRL) at Colorado State University, since that facility has capabilities for testing engines at different climate conditions. EECRL can vary the humidity and temperature of the test lab in order to simulate climates of any part of the country, which is a unique aspect of performing testing at this facility. A question was raised concerning Bryan Willson's affiliation with the University. Amanda Agnew will check into this issue with the TMPWG. Bryan Willson stated that although data would be gathered by his team, analysis and conclusions would not be performed by his team, reducing the chance for bias. Vick Newsom pointed out that the engine test research community is very small, and therefore there are few other choices in engine test contracting. potential problem with testing at this facility would be the effect of the high altitude on the engines, which Bryan Willson stated would have little to no effect on testing for our purposes.

Addressing the CC

Many members were uncertain about how to address the Coordinating Committee on the presentation of the Test Plan. There are several possibilities, such as requesting consensus from the CC, asking for support or endorsement of the Plan, or simply presenting it, stating that the WG will be presenting this to EPA with a request for funding. Amanda Agnew will check with Fred Porter about how to present the Test Plan to the CC; subsequently she and Sam Clowney will revise the presentation accordingly.

On this same note, many details were removed from the Test Plan Presentation in order to avoid issues of debate when presenting to the CC.

Population Subgroup Report on Preliminary MACT Floor

Wayne Hamilton presented the current status of the preliminary MACT floor determination. He suggested that the RICE WG postpone presenting a preliminary MACT floor presentation, to the CC to after the November meeting. He proceeded in making a dry run of the Preliminary MACT Floor Presentation.

Dry Run of Preliminary MACT Floor Presentation and Discussion

The Preliminary MACT Floor Presentation, presented by Wayne Hamilton, is included as Attachment VI.

The topics of discussion which followed included digester gas fired engines as a subcategory, California make and model information, comparisons with other databases for statistical adequacy, four stroke lean burn engines with catalytic reduction, and feasibility of engine subcategorization.

Digester Gas Fired Engines as a Subcategory

Ed Torres suggested that digester gas fired engines should be a separate subcategory, due to the nature of the fuel causing fouling of the catalyst in catalytic control devices.

California Make and Model Information

It was pointed out by the Population Subgroup that when subcategorized by 2/4 stroke and rich/lean burn, California engines seemed to be under represented. The California engines represented 11% of the total database, but showed less than 1% when subcategorized. Jennifer Snyder indicated that this is due to lack of make and model information provided by California, which would have provided a link to engine parameters such as number of stroke and burn type. Don Price stated that he provided engine population information for Ventura County, California which included make and model to Alpha-Gamma. This will be further researched by Alpha-Gamma and the outcome will be provided to the WG at the next meeting.

Comparisons with Other Databases for Statistical Adequacy

One of the tools for determining statistical adequacy of the data is a comparison with the database of Power Systems Research. Brahim Richani gave a brief synopsis of progress with Power Systems Research. He stated that one of the problems with the comparison with this database is the lack of information on whether these engines are non-road or stationary. Bryan Willson stated that he knew of a Power Systems Research report supporting their estimates of the number of stationary engines and non-road engines. Bryan Willson will provide this information to the

Population Subgroup.

It was announced that a comparison will be performed between the API database and the RICE population database. This will be performed on November 11th, and will involve Mike Milliet and Glenda Smith of API, and Alpha-Gamma Technologies.

Four Stroke Lean Burn Engines with Catalytic Reduction

One of the main unresolved issues with the RICE Population Database is that about 50 four stroke lean burn engines in Texas have catalytic reduction as a control device, reflecting a potential MACT floor. However, WG members argue that this control device is impractical, and must be an error in the database. This has been an ongoing issue with the Population Subgroup. Randy Hamilton is currently looking into this issue with the referenced facilities. Brahim Richani stated that a closer look at the referenced engine make and model (when available)indicated that their engines are rich burn units misclassified as lean burn units. Randy Hamilton will report back to the Population Subgroup on this issue.

Feasibility of Engine Subcategorization

Many WG members voiced their opinions that it was premature to present the proposed engine subcategories, based on some apparent data gaps in the current RICE Population Database. Others suggested staying on the ICCR schedule and presenting the current information as "preliminary" at the November CC meeting, since the intuitive conclusions of the WG supports the preliminary MACT floor determination deduction from the database. The consensus of the WG was to defer presenting the preliminary MACT floor determination to a later date, until remaining issues get resolved. Instead, an update of the status of the Preliminary MACT Floor determination will be provided to the CC in a status report, with the following wording: "The RICE Population Subgroup is working on defining a preliminary MACT floor."

Economics WG Presentation on Inter-Work Group Coordination

Walt Brown of the Economics WG made a brief presentation on the data development and analysis schedule of the Economics Analysis WG. One of their activities is to have an Economics WG member attend each of the source WG's meetings on November 20th to discuss data requests for economic and benefits analysis. The Economics WG requested that one RICE WG member be assigned to interact with the Economics WG. The selection of this member will be performed at the November 20 RICE WG meeting.

Model Plants Development

One of the next steps for the RICE WG is to develop model plants for economic analysis. This encompasses the identification of typical engines and sites and the estimation of national impact and cost effectiveness of regulations on industry. It was decided that the Economics Analysis WG will make a presentation at the next WG meeting regarding model plants development.

Next Meeting

The next Internal Combustion Work Group Meeting will be at the Red Lion Hotel in Houston, Texas on Thursday, November 20, 1997, starting at 8:00 a.m. CST. The meeting will run until 3 p.m., and there will be a working lunch. On the agenda for the next meeting are the following topics:

- * Population Subgroup Update on MACT floor
- * Economic WG Presentation
- * CC Meeting Report
- * Update on changes to ICCR process
- * Project funding report
- * Test sites report
- * Selection of Economic WG liaison
- * Presentation by Mike Horowitz on examples from previous rule developments and funding projects under FACA
- * Emissions Subgroup Update
- * New Source MACT Subgroup Update
- * Next Steps

These minutes represent an accurate description of matters discussed and conclusions reached and include a copy of all reports received, issued, or approved at the October 30, 1997 meeting of the Reciprocating Internal Combustion Engines Work Group.

Amanda Agnew

ATTACHMENT I

LIST OF ATTENDEES

Stationary Internal Combustion Engines Work Group Meeting October 30, 1997 List of Attendees

Amanda Agnew EPA OAQPS Emissions Standards Division

Darrell Bowen CNG Transmission Corporation

Sam Clowney Tenneco Energy

Joseph Derra Waukesha Engine Division

Donald Dowdall Engine Manufacturers Association

Charles Elder General Motors Corporation

Wayne Hamilton Shell E&P Technology Company

William Heater Cooper Energy Services

Jay Martin University of Wisconsin-Madison

Vick Newsom Amoco Production Section

Donald Price Ventura County Air Pollution Control District

Bob Stachowicz Waukesha Engine Division

Ed Torres Orange County Sanitation District

Bryan Willson Colorado State University

Jan Connery Eastern Research Group

Brahim Richani Alpha-Gamma Technologies

Jennifer Snyder Alpha-Gamma Technologies

Linda Coerr Coerr Environmental

Walt Brown Economics Work Group

Mahesh Gundappa Radian International

Jim McCarthy GRI

ATTACHMENT II

OCTOBER 30, 1997 MEETING AGENDA

Tentative Agenda

Reciprocating Internal Combustion Engine Work Group October 30, 1997 Work Group Meeting

Skybird Meeting Center – O'Hare Airport Chicago, Illinois

9:00 – 9:30	Welcome, Meeting Goals (A. Agnew) Agenda Review (J. Connery)
	MEETING GOALS: Work Group Consensus on Test Plan Work Group Consensus on Preliminary MACT Floor Work Group Consensus on Presentations on Test Plan and Preliminary MACT Floor for November Coordinating Committee Meeting
9:30 – 10:00	Report from Emissions Subgroup: (S. Clowney) Review of Changes to Test Plan Since Last Meeting
10:00 – 10:45	Dry-Run of Test Plan Presentation for the November Coordinating Committee
10:45 – 11:30	Discussion & Work Group Consensus on Test Plan & Coordinating Committee Presentation
11:30 – 12:00	WORKING LUNCH AND BREAK
12:00 – 12:30	Report from Population Subgroup: (W. Hamilton) Review of Changes to Preliminary MACT Floor Since Last Meeting
12:30 – 1:15	Dry-Run of Preliminary MACT Floor Presentation for the November Coordinating Committee
1:15 – 2:00	Discussion & Work Group Consensus on MACT Floor & Coordinating Committee Presentation
2:00 – 2:15	BREAK
2:15 – 2:45	Presentation by Schedule Subgroup on Timeline/Tracking Subgroup Requirements (A. Agnew)
2:45 – 3:30	Next Steps (A. Agnew and S. Clowney) -Selection of potential test sites -Determining a testing period -Detection limits on Test Plan -Model plants development -Testing Budget
3:30 – 3:40	Update on Results of Satisfaction Survey (A. Agnew)
3:40 - 3:50	Next Meeting: Schedule and Tentative Agenda Items (J. Connery)
3:45 – 4:00	Review of Flash Minutes (J. Connery and J. Snyder)

4:00 ADJOURN

ATTACHMENT III

BULLET POINT SUMMARY

Summary of ICCR Source Work Group Meeting, October 30, 1997 Internal Combustion Engines Work Group Meeting Skybird Meeting Centre, Chicago, Illinois

Decisions

- Consensus on Test Plan (with modification of addition of dioxin comments to appendix).
- Modifications will be made to Test Plan Presentation (essentially removing details which may raise issues
 of debate).
- There will be no presentation of a preliminary MACT floor at the CC meeting in November. Instead, an update on the status of preliminary MACT floor development will be posted on the TTN prior to the November meeting, with the following wording: The RICE Population subgroup is working on defining a preliminary MACT floor.

Next Meeting

- The next RICE Work Group Meeting will be held at the Red Lion Hotel in Houston, Texas on Thursday, November 20th from 8:00 a.m. to 3:00 p.m. CST. (There will be a working lunch.)
- On the agenda for the next meeting are the following:
 - *Population Subgroup update
 - *Emissions Subgroup update
 - *New Source MACT Subgroup update
 - *CC Meeting Report
 - *Economics WG presentation on Model Plants
 - *Update on changes made to ICCR Process (A. Agnew)
 - *Project funding report, test sites report (A. Agnew)
 - *Selection of Economic WG liaison
 - *Presentation by Michael Horowitz on examples from previous rule developments and funding projects under FACA
 - *Next Steps

Action Items

- Emissions Subgroup: Address dioxin issue in Test Plan appendix.
- Emissions Subgroup: Revise Test Plan Presentation and forward to RICE WG by 11/4/97.
- S. Clowney: Set up teleconference to discuss revised Test Plan Presentation before 11/20 WG Meeting.
- WG: keep a lookout for environmental representation for the RICE WG.
- WG: Choose a RICE WG member to interact with the Economics WG.
- A. Agnew: Discuss next steps for testing with T. Harrison and the possibility of EPA allocation of funds directly to RICE WG.
- A. Agnew: Talk to F. Porter about how to address the CC on Test Plan Presentation (develop final slide).
- A. Agnew: Check with TMPWG on using Colorado State University as a test site for engines.
- A. Agnew/Walt Brown: Ask Economics WG to present an introduction to model plants.
- Population Subgroup: Obtain verification on 4SLB engines with catalytic reduction as a control device (mainly Texas records).
- Bryan Willson: Obtain Power Systems Research report regarding non-road vs. stationary engines for Population Subgroup.
- Alpha-Gamma: Check on California Make and Model information submitted by Don Price.
- D. Price: Identify possible test sites in California.

ATTACHMENT IV

DRAFT TEST PLAN FOR RICE

PLAN TO CONDUCT EMISSIONS TESTING FOR RECIPROCATING INTERNAL COMBUSTION ENGINES

presented to:

Reciprocating Internal Combustion Engine (RICE) Work Group Industrial Combustion Coordinated Rulemaking

presented by:

Emissions Subgroup of the RICE Work Group Industrial Combustion Coordinated Rulemaking

October 27, 1997

RICE Emissions Test Plan DRAFT: October 27, 1997

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1.0 INTRODUCTION

The Reciprocating Internal Combustion Engine (RICE) Work Group has determined that additional hazardous air pollutant (HAP) emissions data are necessary to support the regulatory development process, as described in the "Industrial Combustion Coordinated Rulemaking (ICCR) Organizational Structure and Process" document, dated June 1997. Supporting information is provided in **Appendix A** regarding the Work Group's determination that more emissions data are necessary to support the ICCR rule development for RICE.

In order to obtain additional emissions data (both air toxics and criteria pollutants), the Work Group is recommending this plan for emissions testing of stationary RICE. The RICE Work Group has developed this test plan with the knowledge that resources under ICCR are extremely limited. Therefore, the Work Group has developed this test plan as one that is achievable given the budget constraints within the ICCR process. The Test Plan does not address all the questions that must be answered regarding emissions from RICE and the effectiveness of potential maximum achievable control technology (MACT). However, the results of this test plan will provide additional emissions data and will address key data gaps that have been identified in the EPA ICCR Emissions Database for RICE.

1.1 Components of the Test Plan

The test plan has five components:

Engines, Fuels, and Emission Controls to be Tested
Matrix of Operating Conditions to be Tested
Pollutants to be Measured During Testing
Test Methods to Quantify Emissions
Prioritization

Each of these components is discussed in the sections that follow. A summary table for each emission test proposed is provided in the final section of this test plan.

1.2 Emissions Testing Goals Identified by RICE Work Group

The RICE Work Group has identified the following possible goals for emissions testing under ICCR:

- acquire additional emissions data that can assist the Work Group in determining the effectiveness of after-treatment control devices to reduce formaldehyde and other HAPs:
- acquire additional emissions data that can assist the Work Group in determining the effectiveness of combustion modifications to reduce formaldehyde and other HAPs:
- acquire additional emissions data that can assist the Work Group in determining typical emissions for engines throughout the operating range.

The Work Group has designed the emissions test plan around Goal #1, for the following reasons:

- Emissions data to demonstrate the effectiveness of possible MACT control devices for existing RICE is a data gap in the ICCR Emissions Database for RICE. (see **Appendix A**)
- Understanding of the effects of combustion modifications on HAPs is in its infancy, and would require a very extensive research program to identify potential control techniques, along with confirming testing.

EPA has endorsed the use of ICCR emissions testing dollars to achieve this goal.

In addition, the Work Group has further focused the plan to address the effectiveness of after-treatment control devices on formaldehyde emissions, primarily, and on other HAPs, secondarily. The Work Group will gather emissions data for all HAPs included on the target list of pollutants. However, the control devices to be tested were selected principally for their potential to reduce formaldehyde emissions. The Work Group has added this focus to the test plan for the following reasons:

Formaldehyde is a product of incomplete combustion and generally is the HAP emitted in the greatest quantities from RICE.

The Work Group was able to identify possible maximum achievable control technology (MACT) for formaldehyde based on the results of emissions testing conducted by industry. There is less understanding of possible MACT for other

HAPs.

The test plan also will support Goal #3 in part, since pre-controlled emissions throughout a 16-point test matrix of operating conditions will be recorded during the testing program.

2.0 ENGINES, FUELS, AND EMISSION CONTROLS TO BE TESTED

2.1 Engines

The RICE Work Group recommends that a minimum of four engines be tested under ICCR. Each of the engines selected represents a possible subcategory of engines (see **Table 1**).

Table 1. Engines to be Tested

Engine to be Tested	Possible Engine Subcategory
Clark TLA Turbocharged	2-stroke, gaseous fuel
Caterpillar 3500 Series Turbocharged	liquid-fuel
Waukesha 7042 GL Turbocharged	4-stroke, lean-burn, gaseous fuel
Ingersoll Rand KVG Naturally Aspirated	4-stroke, rich-burn, gaseous fuel

Background information on engine configurations is provided in **Appendix B**.

2.2 Fuels

Diesel fuel has been selected as the liquid fuel to be tested. The Work Group selected diesel fuel because most stationary RICE that use liquid fuels use diesel.

Natural gas has been selected as the gaseous fuel to be tested. The Work Group selected natural gas because most stationary RICE that use gaseous fuels use natural gas.

2.3 Emission Controls

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The Work Group recommends that the engines be tested with emissions control devices that have been identified as possible maximum achievable control technology (MACT). To date, the Work Group has identified oxidation catalysts as possible MACT for leanburn engines. For rich-burn engines, the Work Group has identified non-selective catalytic reduction (NSCR) as possible MACT.

The control devices to be tested are presented in **Table 2**. The Work Group recommends that the Clark, Waukesha, and Caterpillar be tested with oxidation catalysts. The Work Group recommends that the Ingersoll Rand be tested with an NSCR catalyst.

Table 2. Control Devices to be Tested

Engines	Control Device
Clark TLA Turbocharged	oxidation catalyst
Caterpillar 3500 Series Turbocharged	oxidation catalyst
Waukesha 7042 GL Turbocharged	oxidation catalyst
Ingersoll Rand KVG Naturally Aspirated	non-selective catalytic reduction (NSCR)

Since catalyst design, formulation, and age can affect catalyst performance, the RICE Work Group will review each of these factors when selecting sites for testing.

3.0 MATRIX OF OPERATING CONDITIONS TO BE TESTED

The Work Group recommends that the engines be tested throughout the entire operating envelope. The Work Group has developed a 16-point test matrix of operating conditions to be tested (see **Table 3**). The test matrix includes varied speed, torque, air-to-fuel ratio, air manifold temperature, jacket water temperature, timing, and combustion balance as applicable to the specific engine's operating envelope. The tests are organized as follows:

Four corners of the torque / speed envelope (runs 1-4)
Air-to-fuel ratio sensitivity (runs 1, 5-6)

High speed and low load (run 7)

Low speed and high load (run 8)

Air manifold temperature sensitivity (runs 1, 9-10)

Jacket water temperature sensitivity (run s1, 11-12)

Injection or spark timing sensitivity (runs 13-14)

Engine balance sensitivity (runs 1, 15-16)
 Same as run 1, but at limit of acceptable imbalance.

An abbreviated matrix will apply to the engines using diesel fuels due to a reduced ability to vary parameters. Specific settings for the four engines selected are presented in the summary tables in the final section of this test plan. It is estimated that the test matrix will require approximately three days of emissions testing for each engine.

The Work Group recommends that runs 1-14 be conducted with engine balance within the OEM (original equipment manufacturer) specification of good balance. An engine may be in stable operation and not conform to the OEM's balance specification. Engine balance is commonly defined in terms of the difference in peak combustion pressure or exhaust temperature between the highest value and lowest value cylinders of the engine. An engine with acceptable balance has the maximum difference(s) within a set OEM specification. To determine unbalance requires the proper instrumentation to measure these pressures and/or temperatures on the individual cylinders. To unbalance an engine (runs 15-16) requires an engine with the provision to adjust individual cylinder compression or ignition timing.

The Work Group recommends that an engine "expert" be on-site during all testing to ensure that the engine is properly balanced and is being tested in a well-maintained condition. More information on the engine set-up, carrying out the test runs, and data acquisition is provided in **Appendix C**.

Table 3. Matrix of Operating Conditions to be Tested

Run	Speed	Torque	Air-to-Fuel Ratio	Timing	Air Manifold Temperature	Jacket Water Temperature		
1	Н	Н	N	S	S	S		
2	Н	L	N	S	S	S		
3	L	L	N	S	S	S		
4	L	Н	N	S	S	S		
	_				J			
5	Н	Н	L	S	S	S		
6	Н	Н	Н	S	S	S		
7	Н	L		S	S	S		
			Н					
8	L	Н	L	S	S	S		
9	Н	Н	N	S	L	S		
10	Н	Н	N	S	Н	S		
11	Н	Н	N	S	S	L		
12	Н	Н	N	S	S	Н		
13	Н	Н	N	L	S	S		
14	Н	Н	N	Н	S	S		
15	H^1	H ¹	N^1	S ¹	S ¹	S ¹		
16	H^1	H ¹	N^1	S ¹	S ¹	S ¹		
*Notes: H = high-end setting L = low-end setting N = Nominal setting required to satisfy emissions S = set point	H and L to be determined based on operating range and control flexibility.	H, L to be determined based on operating range and control flexibility.	H, L to be determined based on operating range and control flexibility.	H, L to be determined based on operating range and control flexibility.				

IV - 7

¹ Same as Run #1 except with engine at limit of acceptable imbalance.

4.0 POLLUTANTS TO BE MEASURED DURING TESTING

The Work Group recommends that emissions data for both hazardous air pollutants (HAPs) and criteria pollutants be collected before and after emission control devices using two sample-line systems (inlet and outlet). More information on collection of the pollutant information is provided in **Appendix C**.

The HAPs and criteria pollutants to be measured during testing were determined based on the Work Group's list of principal pollutants that are reasonably anticipated to be emitted from the RICE and input on the pollutant lists from Coordinating Committee members and other participants in ICCR. The comments received and the Work Group's response to the comments are provided in **Appendix D**.

Emissions data for the following criteria pollutants will be collected:

carbon monoxide (CO)
nitrogen oxides (NOx)
total hydrocarbons (THC)
particulate matter (PM) (diesel only)

Seven HAP pollutants are included in the test plan for all engines, regardless of fuel:

BTEX (benzene, toluene, ethylbenzene, and xylene) and
three aldehydes (formaldehyde, acetaldehyde, and acrolein).

Naphthalene, 1-3, butadiene, and PAHs are included for natural gas and diesel fuel. In addition, n-Hexane and metals are included for diesel fuel. Chlorinated compounds that were originally included on the pollutant list for natural gas have been removed based on further review of the emissions test data in the ICCR Emissions Database and industry data related to the absence of chlorine in natural gas fuel. More information on the basis for removing the chlorinated compounds is provided in **Appendix D**. A list of pollutants for each proposed test is provided in the final section of this test plan. Diluent gas

(oxygen and carbon dioxide) measurements also will be made.

5.0 TEST METHODS TO QUANTIFY EMISSIONS DURING TESTING

The Work Group recommends the use of emissions test methods that will provide direct measurement and reporting of pollutant concentrations on-site. This approach to the test methods has been selected since it will be necessary to have on-site data to fully evaluate and conduct the matrix of engine operating conditions.

The Testing and Monitoring Work Group provided guidance on the available methods to provide on-site data. Based on the T&M information, the aldehydes, BTEX compounds, n-Hexane, and 1-3, butadiene can be measured with test methods that will provide on-site data. There is no test method for naphthalene and PAHs that will provide on-site data. Therefore, the Work Group recommends that naphthalene and PAH data be collected through laboratory analysis, using CARB 429.

There is no EPA-approved method to measure PM emissions from stationary RICE. The EPA Method 5 is not appropriate for use on RICE due to the small diameter of the RICE stack (less than 0.3 meters) and the variability of the exhaust gases. The only EPA-approved method to measure PM from RICE is ISO Method 8178, which was developed to measure PM from RICE that are non-road, mobile engines.

The RICE Work Group recommends that FTIR be used to collect data on aldehydes, NOx, and CO. The Work Group recommends that the direct-interface GCMS method be used to collect BTEX, n-Hexane, and 1-3, butadiene data. The Work Group recommends that metals for diesel fuel be evaluated through fuel testing. The Work Group recommends that ISO Method 8178 be used to measure PM from the diesel engine to be tested. The Work Group recommends that the testing be conducted to achieve the lowest practical detection limits for all compounds. Preliminary information regarding achievable detection limits is provided in **Table 4**.

The proposed test methods for each proposed emission test are provided in the summaries of proposed emissions tests in the final section of this test plan. More information on sample collection is provided in **Appendix C**.

Table 4. Achievable Detection Limits for Test Methods Identified in RICE Test Plan

Test Method	Sample Time	Pollutants	Achievable Detection Limits
Direct Interface	10 minutes	BTEX	50 ppb
GCMS		1,3-Butadiene	75 ppb
		Hexane	75 ppb
FTIR	10 minutes	BTEX	> 3 ppm
		1,3-Butadiene	> 3 ppm
		Hexane	> 10 ppm
		Formaldehyde	100 ppb
		Acetaldehyde	100 ppb
		Acrolein	100 ppb
		NOx	2-10 ppm
		CO	2-10 ppm
		CH4	2-10 ppm
CARB 429	1 hour**	PAH	see note**
		Naphthalene	see note**
EPA Method 25A	Continuous***	THC	1-5 ppm
		CH4	1-5 ppm
ISO 8178	To be provided by	PM	To be provided by Bill
	Bill Passie at the		Passie at the 10/30
	10/30 meeting		meeting

^{*} Grab sample with 2-4 week analysis time also requires 16 SUMMA Canisters for each location.

6.0 PRIORITIZATION

The RICE Work Group has designed this Test Plan to give priority to emissions testing for the four engines identified. The Work Group recommends that emissions testing be

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^{**} Grab sample with 2-4 week analysis time. Detection limits dependant on sample time. A longer sample time will yield lower detection limits.

^{***} Samples are run directly to a Flame Ionization Detector (FID) and measurements are made instantaneously.

conducted as described in this Test Plan.

7.0 **SUMMARY OF PROPOSED EMISSIONS TESTS**

7.1 Test #1: Clark TLA

Engine Subcategory:	2-stroke, le	ean-burn, ga	seous fuel			
Engine to be Tested:		Turbochar				
Fuel:	Natural Gas					
Control Device:	Oxidation	Catalyst				
Pollutants to be Measured:	Criteria Po					
	NOx, CO	O, THC				
	Hazardous	Air Pollutant	s:			
		Toluene, Eth	•	•	1	
		ehyde, Acetal	•			
		diene, Napht		S		
Test Methods to be Used:		face GCMS				
		Toluene, Eth	nylbenzene, a	nd Xylene(s)	1	
	1-3, Buta	idiene				
	FTIR for:					
		ehyde, Acetal	dehyde, Acro	olein		
	NOx, CO Method 429					
		ene, PAHs				
		A for: THC	and CH4			
Operating Conditions to be	Speed Speed	Torque	Air-to-	Timing	Air	Jacket
Tested:	Бреса	Torque	Fuel	Tilling	Manifold	Water
rested.			Ratio		Temp.	Temp.
			Tuno		remp.	remp.
Run 1	Н	Н	N	S	S	S
Run 2	H^1	L^1	N^1	S^1	S^1	S^1
Run 3	L^2	L^2	N^2	S^2	S^2	S^2
Run 4	$L^{1,2}$	$H^{1,2}$	$N^{1,2}$	S ^{1,2}	S ^{1,2}	S ^{1,2}
Run 5	Н	Н	L	S	S	S
Run 6	Н	Н	Н	S	S	S
Run 7	H^2	L^2	H^2	S^2	S^2	S^2
Run 8	L^2	H^2	L^2	S^2	S^2	S^2
Run 9	Н	Н	N	S	L	S
Run 10	Н	Н	N	S	Н	S
Run 11	Н	Н	N	S	S	L
Run 12	Н	Н	N	S	S	Н
Run 13	Н	Н	N	L	S	S
Run 14	Н	Н	N	Н	S	S
Run 15	H^3	H ³	N ³	S^3	S^3	S^3
Run 16	H^3	H^3	N^3	S^3	S^3	S^3
	$L^4 = 270$	$L^{4,5} = 70$	$N^6 = 0.25$	S = 4.5	$S^7 = 100$	$S^8 = 150$
	$H^4 = 300$	$H^{4,5} = 100$	$L^6 = 0.22$ $H^6 = 0.28$	L = 2 $H = 7$	$L^7 = 80$ $H^7 = 120$	$L^8 = 140$ $H^8 = 160$
			11 0.20		11 120	11 100
Runs #2 and #4 are not applicable if the engine at	4	. 11		1 1 11	11 :	11 1

Runs #2 and #4 are not applicable if the engine at the test site is running a pump or blower, since the torque absorbed by a pump or blower is generally determined by speed. Runs #3, #4, #7, and #8 are not applicable if the engine at the test site is running a synchronous generator, since synchronous generators do not vary speed. Same as Run #1 except with engine at limit of acceptable imbalance.

Depending on site and operating conditions, speed and torque range may vary.

If unit has ambient rating controls capability, high torque value may be up to 124%.

Fuel/air equivalence ratio for this two-stroke cycle engine is based on total airflow through engine, not trapped air.

JWT setpoint is based on normal operating practices, but may vary depending on site-specific conditions.

IT setpoint is based on pipeline quality natural gas. IT is a function of engine speed and AMT.

Test #2: Caterpillar 3500 Series 7.2

Engine Subcategory:	Liquid Fue	el				
Engine to be Tested:			s Turbocharg	ed		
Fuel:	Diesel Fuel					
Control Device:	Oxidation Catalyst					
Pollutants to be Measured:	Criteria Pollutants:					
	NOx, CO	O, THC, and	d PM			
	Hazardous	s Air Polluta	ants:			
			Ethylbenzene, 1			
		• /	taldehyde, Acı			
			diene, Naphth			
			yllium, Cadm			,
			ercury, Nicke			
Test Methods to be Used:			IS Method for			
			Ethylbenzene,	Xylene(s),		
	n-Hexane, FTIR for:	1-3, Butadi	ene			
		lahvda Aca	taldehyde, Acı	rolain NOs	z and CO	
			thalene, PAHs		s, and CO	
		A for THC	marche, i Alis	•		
		or Particula	ate Matter			
		ng for Metal				
Operating Conditions to be	Speed	Torque	Air-to- Fuel	Timing	Air	Jacket
Tested:			Ratio		Manifold Temp.	Water Temp.
Run 1	Н	Н	N	S	S	S
Run 2	H^1	L^1	N^1	S^1	S ¹	S ¹
Run 3	L^2	L^2	N^2	S^2	S^2	S^2
Run 4	$L^{1,2}$	$H^{1,2}$	N ^{1,2}	$S^{1,2}$	S ^{1,2}	$S^{1,2}$
Run 5			Not Appl	icable		
Run 6			Not Appl			
Run 7			Not Appl	icable		
Run 8			Not Appl	icable		
Run 9	Н	Н	N	S	L	S
Run 10	Н	Н	N	S	Н	S
Run 11	Н	Н	N	S	S	L
Run 12	Н	Н	N	S	S	Н
Run 13			Not Appl	icable		
Run 14			Not Appl			
Run 15	H^3	H^3	N^3	S^3	S^3	S^3
Run 16	H^3	H^3	N^3	S^3	S^3	S^3
	$L^{4,5} = 1000$	$L^5 = 70$	N = 0.68	S = 28	$S^6 = 130$	$S^7 = 160$
	$H^{4,5} = 1200$	$H^5 = 100$	(7.5% O2)	L = 26	$L^6 = 120$ $H^6 = 140$	$L^7 = 155$ $H^7 = 165$
			L = 0.63 (8.5% O2)	H = 30	п = 140	п = 105
			H = 0.74			
Puns 2 and 4 are not applicable if the engine at the			(6.5% O2)	L		

Runs 2 and 4 are not applicable if the engine at the test site is running a pump or blower, since the torque absorbed by a pump or blower is generally determined by speed. Runs 3, 4, 7, and 8 are not applicable if the engine at the test site is running a synchronous generator, since synchronous generators do not vary speed.

Same as Run #1 except with engine at limit of acceptable imbalance.

Depending on rating of separable compressor unit, speed values may vary between 700 – 1200 rpm.

Depending on site and operating conditions, speed and torque range may vary.

AMT totally depends on type of cooler configuration.

JWT setpoint is based on normal operating practices, but may vary depending on site-specific conditions.

IT setpoint is based on diesel fuel.

7.3 Test #3: Waukesha 7042 GL

Engine Subcategory:	4-stroke, le	ean-burn, g	gaseous fuel			
Engine to be Tested:	Waukesha 7042 GL Turbocharged					
Fuel:	Natural Gas					
Control Device:	Oxidation Catalyst					
Pollutants to be Measured:	Criteria Po	ollutants:				
	NOx, CO	O, THC				
	Hazardous	Air Pollu	tants:			
	Benzene	, Toluene,	Ethylbenzene, 1	Xylene(s)		
		-	etaldehyde, Acı			
			phthalene, PAI			
Test Methods to be Used:			MS Method for			
			Ethylbenzene, 2	Xylene(s)		
	1-3, But	adiene				
	FTIR for:			1.1 NO	a a	
		-	etaldehyde, Acı		CO	
	Method 42 Method 25		nthalene, PAHs			
Operating Conditions to be	Speed	Torque	Air-to- Fuel	Timing	Air	Jacket
Tested:	Speeu	Torque	Ratio	Tilling	Manifol	Water
rested.			Ratio		d Temp.	Temp.
Run 1	Н	Н	N	S	S S	S S
Run 2	H ¹	L^1	N^1	S^1	S ¹	S^1
Run 3	L^2	L^2	N^2	S^2	S^2	S^2
Run 4	$L^{1,2}$	$H^{1,2}$	$N^{1,2}$	S ^{1,2}	$S^{1,2}$	$S^{1,2}$
Run 5	Н	Н	L	S	S	S
Run 6	Н	Н	Н	S	S	S
Run 7	H^2	L^2	H^2	S^2	S^2	S^2
Run 8	L^2	H^2	L^2	S^2	S^2	S^2
Run 9	Н	Н	N	S	L	S
Run 10	Н	Н	N	S	Н	S
Run 11	Н	Н	N	S	S	L
Run 12	Н	Н	N	S	S	Н
Run 13	Н	Н	N	L	S	S
Run 14	Н	Н	N	Н	S	S
Run 15	H ³	H^3	N ³	S^3	S^3	S^3
Run 16	H^3	H^3	N^3	S^3	S^3	S^3
	$L^{4,5} = 1000$	$L^4 = 70$	N = 0.57	$S^8 = 10$	$S^5 =$	$S^7 = 180$
	$H^{4,5} =$	$H^4 =$	(9.8% O2)	$L^8 = 6$	130	
	1200	100	L = 0.53 (10.7% O2)	$H^8 = 14$	$L^5 =$	
			H = 0.62		120	
			(8.7% O2)		$H^5 =$	
Runs 2 and 4 are not applicable if the engine at the					140	

Runs 2 and 4 are not applicable if the engine at the test site is running a pump or blower, since the torque absorbed by a pump or blower is generally determined by speed. Runs 3, 4, 7, and 8 are not applicable if the engine at the test site is running a synchronous generator, since synchronous generators do not vary speed.

Same as Run 1 except with engine at limit of acceptable imbalance.

Depending on rating of separable compressor unit, speed values may vary between 700 – 1200 rpm.

Depending on site conditions, speed and torque range may vary.

AMT setpoint depends on type of cooler configuration.

JWT setpoint is fixed control per thermostat. May not be changed by user-defined control setpoint. IT setpoint is based on pipeline quality natural gas.

Test #4: Ingersoll Rand KVG **7.4**

Engine Subcategory:	4-stroke, rich-burn, gaseous fuel					
Engine to be Tested:	Ingersoll Rand KVG Naturally Aspirated					
Fuel:	Natural Gas					
Control Device:			c Reduction	(NSCR) 3-V	Vay Catalys	t
Pollutants to be Measured:	Criteria Po					
	NOx, CO), THC s Air Polluta	mta.			
			mıs: thylbenzene	Xvlene(s)		
			aldehyde, A			
			hthalene, PA			
Test Methods to be Used:			S Method fo			
			thylbenzene	, Xylene(s)		
	1-3, Buta FTIR for:	adiene				
		lehvde Acet	aldehyde, A	crolein NO	x CO	
	Method 42		aracity ac, 11	ci oicin, 1 (0)	1,00	
		alene, PAHs				
		A for THC ar				
Operating Conditions to	Speed	Torque	Air-to- Fuel Ratio	Timing	Air Manifold	Jacket Water
be Tested:					Temp.	Temp.
Run 1	Н	Н	N	S	S	S
Run 2	H^1	L^1	N^1	S^1	S^1	S^1
Run 3	L^2	L^2	N^2	S^2	S^2	S^2
Run 4	$L^{1,2}$	$H^{1,2}$	$N^{1,2}$	$S^{1,2}$	$S^{1,2}$	S ^{1,2}
Run 5	Н	Н	L	S	S	S
Run 6	Н	Н	Н	S	S	S
Run 7	H^2	L^2	H^2	S^2	S^2	S^2
Run 8	L^2	H^2	L^2	S^2	S^2	S^2
Run 9	Н	Н	N	S	L	S
Run 10	Н	Н	N	S	Н	S
Run 11	Н	Н	N	S	S	L
Run 12	Н	Н	N	S	S	Н
Run 13	Н	Н	N	L	S	S
Run 14	Н	Н	N	Н	S	S
Run 15	H^3	H^3	N^3	S^3	S^3	S^3
Run 16	H^3	H^3	N^3	S^3	S^3	S^3
	$L^4 = 270$	$L^4 = 70$	S = 1.00	$S^7 = 15$	See Note ⁵	$S^6 = 155$
	$H^4 = 300$	$H^4 = 100$	L = 0.95	$L^7 = 12$		$L^6 = 145$
Runs 2 and 4 are not applicable if the engine at the	toot oito io mumino	o mumm on blosses	H = 1.05	$H^7 = 18$	blorron io cono	$H^6 = 165$

Runs 2 and 4 are not applicable if the engine at the test site is running a pump or blower, since the torque absorbed by a pump or blower is generally determined by speed. Runs 3, 4, 7, and 8 are not applicable if the engine at the test site is running a synchronous generator, since synchronous generators do not vary speed. Same as Run 1 except with engine at limit of acceptable imbalance.

Depending on site and operating conditions, speed and torque range may vary.

AMT totally dependent on ambient temperatures. 20 degree swing in temperature desirable for testing.

JWT setpoint is based on normal operating practices, but may vary depending on site-specific conditions.

IT setpoint is based on pipeline quality natural gas and may vary with certain ambient and operating parameters.

APPENDIX A:

Information on Work Group's Determination that More HAP Emissions Data are Necessary to Support the ICCR Rule Development The RICE Work Group has concluded that additional emissions data are necessary to support the ICCR rule development. This conclusion was reached as a result of the Work Group's review of emissions data available to the ICCR process in the EPA ICCR Emissions Database for RICE.

The RICE Work Group established the Emissions Subgroup in February 1997 to review the emissions data in the EPA ICCR Emissions Database for RICE. Members of the Subgroup reviewed the emissions test reports that were the source of the ICCR emissions data for RICE.

In March 1997, the Subgroup reported on the results of their review. The Subgroup noted that the emission levels reported in the ICCR Emissions Database for RICE were highly variable. The Subgroup speculated that the variability could be attributed to two possible causes:

- reported formaldehyde levels in some cases may be artificially low due to interference with DNPH-based test methods, and
- emissions may be affected by the operating condition of the engine when tested

When the Subgroup reviewed the test reports to determine if the variability could be explained by the operating conditions of the engines, the Subgroup discovered that many of the test reports lacked key information about engineering and operating parameters that could affect HAP emissions. For example, the manufacturer and model of the engine were often lacking in test reports. Whether the engine was a 2-stroke or 4-stroke cycle was lacking. The air-to-fuel ratio was often lacking, as was the horsepower and speed (rated and as tested). The Subgroup concluded that there was insufficient information in the test reports to account for the unexplained variability in the emissions data included in the ICCR Emissions Database for RICE. The Subgroup also concluded that, apparently, there is no existing data for testing a single engine over the entire envelope of operating conditions.

The RICE Work Group has not made a final decision on the use of data in the ICCR Emissions Database for RICE – some of the data may be useful in the ICCR process, while, clearly, some of the data will be inadequate for use in ICCR. However, the RICE Work Group has identified key emissions data gaps, including the following:

- the effect of operating conditions on emissions, and
- the effectiveness of possible MACT control devices in reducing HAP emissions.

EPA also has noted the deficiencies in the ICCR Emissions Database for possible MACT control devices. In an October 1, 1997 memorandum to the Emissions Subgroup, Amanda Agnew of EPA notes that although there is some data in the database for before and after controls, the data for NSCR "correspond to a limited number of pollutants and high detection limits (FTIR with a 0.5 ppm detection limit)," and the data for oxidation catalysts have the following limitations, "1) the unavailability of emission data necessary to estimate a representative control efficiency, and 2) only a small portion of the pollutants were measured before and after controls."

Given the critical data gaps, the RICE Work Group agreed, by consensus, that additional emissions data are needed to support the ICCR rule development.

APPENDIX B: Background Information on Engines and Emission Controls

1.0Engines to be Tested

1.1Types of Engines

Stationary reciprocating internal combustion engines come in a wide variety of makes and models utilizing both liquid and gaseous fuels in diverse applications. The various types can be described according to:

operating cycle scavenging cycle fuel type

A brief description of each of these categories is provided below.

1.1.1 Operating Cycle

There are two operating cycles in common use for reciprocating internal combustion engines: spark ignition (SI), also known as otto cycle, and compression ignition (CI) also known as the diesel cycle. The SI cycle uses lower compression ratios than does the CI cycle and relies on a mechanical spark to ignite the fuel mixture in the cylinder. The CI cycle uses high compression and the resultant high temperatures to effect autoignition of the fuel in the cylinder. The intake process for both SI and CI cycles, including the fuel mixing process and ignition timing, impacts the initiation and the rate of combustion, which, in turn, may impact air toxics formation. A more detailed description of both operating cycles is provided below.

1.1.1.1 Spark Ignition (SI)

SI engines utilize a "spark" generated by a spark plug and associated electronics to initiate combustion. Traditionally, one or more of these spark plugs were mounted directly in the combustion chamber. While simple, when applied to larger bore engines, such "Open Combustion Chamber" (SI-OCC) systems result in significant combustion instability and can operate only at moderately lean air/fuel ratios. To extend the lean limit (and thereby reduce NO_x emissions while improving efficiency) Original Engine Manufacturers (OEMs) introduced two-stage combustion including a rich initial phase that has sufficient energy to light off the very lean secondary phase. Usually the rich

phase is ignited by the spark in a "Pre-Combustion Chamber" (SI-PCC).

Recently, several after-market manufacturers have offered alternative electrical based ignition systems such as plasma jets. Typically these High-Energy (HE) ignition systems operate in an OCC, and will be referred to as HE-OCC in this document.

1.1.1.2 Compression Ignition (CI)

Compression Ignition engines operate at significantly higher compression ratios than SI engines, with the resultant heat of compression raising the temperature of the trapped air or air/fuel charge to ~800°F or more. Fuel (usually liquid) injected into this hot compressed gas then spontaneously vaporizes, disassociates and ignites. Often CI engines are referred to as "diesel" engines after the originator and patent holder of the method¹. While some vehicular diesel engines utilize a pre combustion chamber to assist in ignition, particularly at part load, all large stationary CI "diesels" have OCCs to maximize efficiency and performance.

The other major type of CI engine scavenges or injects gaseous fuels into the combustion chamber with the fresh air charge and then utilizes a small "pilot injection" of liquid fuel (usually No. 2D) to ignite the mixture. Typically called "dual fuel" or "gasdiesel" engines, the less expensive gaseous fuel usually provides 90-99% of the input energy while the more expensive liquid fuel provides the balance. Originally, dual fuel engines were simple conversions of OCC diesel engines which maintained the ability to operate on "full diesel" (i.e. 100% liquid fuel). While offering favorable NO $_{\rm x}$ emissions in this configuration (4-5 g/BHP-HR), subsequent regulatory pressure to further reduce emissions resulted in several OEMs offering such engines fitted with PCCs to reduce the pilot fraction to $\approx 1\%$ or less.

By their nature (i.e. ignition via heat of compression), all stationary CI engines are inherently "lean burn", usually utilizing turbochargers and intercoolers to achieve the desired fresh air density.

1.1.2 Scavenging Cycles

¹ Rudolph Diesel originally wanted to utilize coal dust as the fuel but soon changed to liquid fuels when the former burned uncontrollably and proved excessively abrasive.

Reciprocating internal combustion engines utilize either 2-stroke cycle (2SC) or 4-stroke cycle (4SC) scavenging. The efficacy of the scavenging cycle will impact the trapped air/fuel charge in turn impacting air toxics formation. A summary of the various scavenging cycles and equipment configurations is provided below.

1.1.2.1 4-Stroke Cycle

4SC are the most familiar engine type due to their use in vehicular applications. A 4SC engine undergoes four distinct events or "strokes". Each cycle consists of; intake, compression, power and exhaust. Due to the pumping action of the intake and exhaust strokes, 4SC engines are self-aspirating or "scavenging". 4SC engines operating at fresh air charge densities induced only by this inherent pumping action are often referred to as Naturally Aspirated (NA). Inasmuch as maximum power delivery is limited by the air supply, 4SC NA engines tend to operate near or slightly rich of stoichiometry, hence the appellation "rich burn".

In general, financial and performance considerations require that large (>500 BHP) stationary 4 SC engines operate at specific outputs 2-4 times that obtainable with NA alone. Therefore these engines utilize an auxiliary air compressor to increase the charge density at the engine intake. The most common method is to utilize an exhaust-gas-driven turbine to drive the compressor, usually called a "turbocharger". In addition, to maximize the fresh air charge density, most 4SC turbocharged (4 SC TC) engines utilize an aftercooler or intercooler to remove the heat of compression from the fresh air charge. Typically, mechanical and/or thermal loading limits the output of 4SC TC engines. 4 SC TC engines can operate from rich of stoichiometry to more than twice as lean as stoichiometry (over 100% excess combustion air). A common method used to differentiate between "rich burn" and "lean burn" engines is with percentage oxygen in the exhaust stream. Several regulatory agencies have adopted a value of 4% oxygen in the exhaust as the defining limit for "rich burn" engines. An engine with more than 4% exhaust oxygen is classified as "lean burn". In point of fact, most "lean burn" engines manufactured today contain at least 7% exhaust oxygen.

1.1.2.2 2-Stroke Cycle

² The word scavenge in this use refers to the removal of spent exhaust gases and their replenishment with a fresh air charge.

To maximize power output/density, 2SC engines eliminate the intake and exhaust "pumping" strokes of 4SC engines, retaining only the compression and power strokes. Consequently, an auxiliary device is required to "scavenge" the engine. In their simplest form this may consist of pumping off the underside of the piston or the addition of one or more scavenging pump cylinders to the same crankshaft connecting the power cylinders. In more sophisticated applications gear or motor driven blowers may supply scavenging air. Typically, due to inherent limitations in 2SC scavenging, these pump scavenged (2SC PS) or blower scavenged (2SC BS) 2SC engines operate somewhat lean of stoichiometric and are also classified as "lean burn".

Like 4SC, financial and performance considerations (in particular the parasitic load of crank driven pumps/blowers), require that larger more modern stationary 2 SC engines utilize turbochargers and intercoolers to increase charge air density and hence specific output. 2SC TC engines typically operate lean of stoichiometric conditions and therefore, are known as lean-burn engines.

1.1.3 Fuel Type

Fuel type and associated mixing impact initiation, rate and completeness of combustion, which in turn impacts air toxics formation. Stationary internal combustion engines utilize either liquid or gaseous fuels.

1.1.3.1. Liquid Fuels

With the exception of extremely small co-generation applications (≈<100 kW) liquid fueled SI engines are seldom utilized in stationary applications. Rather, all stationary liquid fueled engines operate on the CI cycle. However, due to the simplicity and robustness of this ignition method, CI engines can operate on a wide variety of liquid fuels ranging from light distillates such as No. 2 fuel oil to residuals from the refining process which are virtually solid at room temperature, sometimes called residual or "heavy" fuel.

1.1.3.2 Gaseous Fuels

Most stationary SI engines operate on gaseous fuels while many stationary CI engines utilize gaseous fuels as the primary energy input. In both cases, most engines use either field or pipeline-quality Natural Gas (NG).

A number of SI and CI engines, usually in "co-generation" applications, operate on other gaseous fuels typically the by-product of some unrelated process. These include "Digester Gas" (DG) from the treatment of wastewater, "Process Gas" (PG) from chemical refining processes and "Landfill Gas" (LFG) from solid waste in landfills.

1.2 Driven Equipment

While the driven equipment generally does not impact air toxics formation per se, the driven equipment does affect the operating speed and torque profile. In particular, operation at high speeds and low torque may encourage air toxics formation while reduced speed and high torque operation can reduce air toxics formation.

1.2.1 Reciprocating compressors

Probably the most common application of stationary engines, engine driven reciprocating compressors are utilized in the "Oil & Gas" industry to gather and process natural gas and in the "Natural Gas Pipeline" to transport natural gas to end users. Typically these engines operate over a range of varying speed (≈80-100% of rated) and torque (≈90-120%). Depending on various parametric settings (i.e. air/fuel, ignition timing, etc.) over the operable range of speed and torque, air toxics formation could vary considerably. Therefore air toxics testing of engines driving reciprocating compressors should minimally include the four speed/torque corners (i.e. max speed/max torque, min speed/min torque, etc.).

1.2.2 Generators

The next most common application, synchronous AC generators driven by stationary engines, is utilized to:

provide prime power in remote locations (i.e. Hawaii, Alaska, etc.)
provide peak/municipal power to the local grid in populated areas
"co-generate" power in conjunction with waste heat recovery with the possibility
to provide excess power to the local grid in populated areas
provide emergency power for hospitals, airports, data centers, nuclear power
plants, and other facilities.

AC generator drives must operate at fixed (synchronous) speed. Therefore, only the torque varies, typically over the range of 75-100% of rated. Other than air/fuel ratio and spark timing on gaseous-fueled engines, parametric variation tends to be limited.

Air toxics emissions should be tested at minimum and maximum torque and at possible timing extremes.

1.2.3 Miscellaneous

After reciprocating compressors and generators, most remaining stationary engines drive rotating compressors, blowers, pumps etc. In general, these machines follow a quadratic relationship between speed and torque (i.e. the torque absorbed is proportional to the square of the speed). Worst case air toxics formation should generally occur at either the minimum or maximum normal operating speed.

2.0 Emission Control Devices to be Tested

In general, emissions control strategies for stationary internal combustion engines focus on NO_x reduction, either by altering the combustion process or exhaust after-treatment. None of these strategies currently focus on the formation/reduction of air toxics.

2.1 Altered Combustion Process

Most larger "lean burn" stationary reciprocating engines subject to emissions limitations utilize some form of altered combustion process to reduce NO_x emissions, which could also impact (most likely increasing) the formation of air toxics. This usually includes parametric adjustments to lean out the air/fuel mixture, often in conjunction with PCCs on SI engines to obtain minimum NO_x . Other NO_x reducing parametric adjustments include retarded injection or ignition timing and reduced charge temperatures.

A few engines may employ other forms of combustion modification including Exhaust Gas Recirculation (EGR) or Water Injection (WI), the latter on diesels only.

2.2 Exhaust After-Treatment

In some applications, stationary reciprocating engines may utilize exhaust gas after-treatment to reduce emissions, again primarily NO_x . This generally consists of a catalytic device.

The three principal catalyst technologies that have been applied to stationary IC engines are:

- 1) Selective catalytic reduction, (SCR) which injects a "reducing agent" (typically ammonia, NH₃) into the exhaust stream upstream of the catalyst to "extract oxygen" from NOx compounds, transforming them into molecular nitrogen, N₂.
- 2) Non-selective catalytic reduction, (NSCR) is used on "rich-burn" engines that can operate at approximately stoichiometric (chemically correct) air/fuel ratios. NSCR catalysts rely on the engine to produce sufficient carbon monoxide (CO) to act as a reducing agent to extract oxygen from the NOx compounds. Maintaining the proper CO/NOx ratio for proper operation requires very precise air/fuel control.
- 3) Oxidation catalysts are used on lean burn engines to reduce the CO that is formed as a product of partial combustion in very lean engines.

The primary HAPs constituent from natural gas engines is formaldehyde, CH₂O, which is formed when conditions do not allow methane to oxidize completely. Formaldehyde is a product of partial combustion, as is CO. The removal of formaldehyde requires the use of a catalyst that promotes further oxidation. SCR catalysts are not expected to be effective in reducing formaldehyde since they are formulated to enhance reduction reactions only. NSCR catalysts are formulated to enhance both reduction and oxidation reactions. It is therefore expected that both NSCR and oxidation catalysts will exhibit some effectiveness in oxidizing formaldehyde. This has been confirmed in the limited field testing that has been conducted to date.

NSCR catalysts appear to be particularly effective for two reasons: 1) engines operating with stoichiometric air/fuel ratios operate with particularly high in-cylinder temperatures which tend to destroy formaldehyde in the combustion chamber, and 2) engines operating at stoichiometric conditions have hot exhaust temperatures which keeps the catalyst in its optimum temperature range for high efficiency. The combination of low "engine-out" HAPs emissions (although NOx levels are high for stoichiometric operation) and high catalyst efficiency should combine to produce effective oxidation of formaldehyde. NSCR catalysts are the most common catalysts for stationary engines, and are applied primarily for NOx control.

The application of oxidation catalysts is less common, but they are used when CO levels from lean burn engines must be reduced. Lean burn engines can have high

specific emissions of formaldehyde due to the cool combustion process and a high degree of flame quenching in the cylinder. Unfortunately, the cool combustion temperatures, which tend to raise formaldehyde levels, can also suppress catalyst efficiency. The exhaust stream of a lean burn engine is colder than that of a "rich-burn" (approximately stoichiometric) engine; this suppresses the efficiency of the catalyst. One of the most challenging applications will be for lean-burn two-stroke cycles, which utilize large amounts of scavenging air. High scavenging rates can drastically reduce the exhaust temperatures. The cool exhaust / catalyst temperatures are expected to make the lean-burn 2-stroke cycle engine the most difficult application. Oxidation catalysts in use have primarily been formulated for oxidation of CO, and have not been optimized for oxidizing formaldehyde or other hydrocarbons. It has been shown that oxidation catalysts can be applied to lean-burn engines to reduce formaldehyde, but do not produce the high reduction efficiencies seen with NSCR catalysts on rich-burn engines due to the differences in exhaust temperatures. If an NSCR catalyst is used on a lean-burn engine, it will promote oxidation, but will have very poor NOx reduction efficiency. Oxidation catalysts are preferred over NSCR catalysts for lean-burn engines.

The efficiency of catalytic after-treatment controls on air toxics is uncertain. In some situations beneficial oxidation of air toxics may occur. However, before and after testing is necessary for verification.

APPENDIX C: Engine Set Up, Execution of Test Runs, and Data Acquisition

1.0 Roles / Responsibilities

Relevant roles during the test include the following:

Test Director

The Test Director will be an engine expert approved by the RICE Work Group. The test director will coordinate all aspects of the test including engine operation, analyzer operation and calibration and assessment of the stability and suitability of engine performance. The test director will review and define required engine maintenance, tuning or adjustment and convey those requests to the Plant Liaison. The test director will elect when to start and stop the test runs and then assess the suitability of each individual run. The test director will generate, review and distribute all final Test Condition Summary Data Sheets and associated archives.

Performance Analyst

The performance analyst will perform analysis of the power cylinder balance and combustion stability and the compressor cylinder horsepower as requested by the test director. The analyst will also assist plant staff in balancing of the power cylinders and diagnosis of any combustion performance aberrations.

RM Operator

The RM operator will maintain and operate all criteria analyzers and related equipment up to and including the stack probe. The RM operator will coordinate pre and post test calibrations with the test director. The RM operator will also perform all post test drift correction calculations and provide the test director with all final drift corrected emissions values.

FTIR Operator

The FTIR operator will maintain and operate the FTIR and all related equipment after the stack probe. The FTIR operator will coordinate pre and post test calibrations with the test director. The FTIR operator will also perform all post test drift correction calculations and provide the test director with all final drift corrected emissions values.

Plant Liaison

Provided by the host company, the plant liaison will coordinate engine loading with gas control, direct the plant operators to set the engine to the desired condition, and arrange for the execution of any maintenance requested by the test director. The plant liaison is responsible for ensuring the engine and auxiliaries operate in a safe

manner that will not compromise their life or operability or endanger the test team.

2.0 Engine Set Up and Testing Conditions

2.1 Pre-test Preparation

At the beginning of each test day, the RM & FTIR operators will perform preliminary calibration of their instruments. The plant liaison will arrange for the calibration of all engine sensors as requested by the test director. The test director will walk down the engine and all systems with the plant liaison to ensure the unit is properly prepared for testing.

2.2 Engine Set-up

Prior to establishing a new test condition, the test director will review the desired test condition with the plant liaison, who in turn will coordinate setting of the engine and auxiliaries to the desired condition.

The test director will then monitor engine operating and emissions parameters and assess stability and suitability of engine performance. The test director will define any required special engine adjustments and, when satisfied, direct the performance analyst to collect a set of readings. Reviewing the results, the director will define any required corrective action. Once satisfied, the test director will begin preparations for a test run.

2.3. Test Run

Once satisfied with the engine set-up, and confident the engine is operating at steady state at the desired condition, the test director will notify the RM and FTIR operators to perform calibrations (as required). Once complete, the test director will begin collecting 10-minute data sets with the DBDAQ, monitoring engine performance and engine speed and load stability throughout. The director will continue to collect data sets until at least three satisfactory runs are obtained at the desired test condition. Upon completion of all runs for a given condition (or as required) the test director will notify the RM and FTIR operators to perform post-calibrations (as required) to reestablish drift correction factors.

Upon completion of each test condition, the test director will generate and distribute a preliminary Test Condition Summary Data Sheet. At the end of each day, the RM and FTIR operators will generate final drift corrected emissions values which the test director

will then incorporate in the final Test Condition Summary Data Sheet.

2.4 Initial Baseline Testing

2.4.1 Engine Preparation, Instrumentation Setup, Calibration and Validation

Prior to initiation of the testing, confirm all scheduled maintenance for the engine and auxiliaries is up to date. Confirm that the engine is in a reasonable, repeatable state of health and tune consistent with good operating practices. Pay particular attention to the condition of the ignition/injection system. Install new spark plugs, replace or rebuild precombustion chamber check valves, clean and pop test fuel injector nozzles, etc., as applicable. All engine adjustments, ignition/injection timing, fuel system, air system, etc., should be set per the manufacturer's specifications.

Any additional sensors that are required for the testing must be installed. Calibrate all sensors providing engine control, performance and emissions parameter sensors. Confirm proper indication of each sensor value at the DBDAQ.

Start and operate the engine at rated speed and torque. Monitor all engine control, performance and emissions parameter sensor values and confirm credibility/validity. Perform hand calculations and cross checks of all calculated parameters such as fuel flow, BHP, BSFC, exhaust flow, emissions mass rates, etc. Take corrective action as required.

2.4.2 Engine Control System Shakedown

Operate the engine at various extremes of operation, including the four corners of the torque / speed map as defined in the matrix of operating conditions.

At each condition, monitor the various control, performance and emissions parameters including speed, intake manifold temperature, intake manifold pressure, IWT, jacket water temperature, fuel flow, exhaust O2, and others specified by the RICE Work Group. Confirm that the automation can control the engine over the operating range with sufficient stability (commonly defined as an acceptable tolerance of speed and/or load variation around the desired mean values) to obtain repeatable data. Investigate and resolve any instabilities, inconsistencies, problems, etc.

2.4.3 Engine Performance Repeatability Test

Operate the engine in stable conditions at rated speed and torque (baseline condition). Collect three or more test runs. Disturb the engine by altering one or more control

parameters and operate at that condition for at least one hour. Return the unit to rated speed and torque. Once equilibrium is obtained, collect three or more test runs. Repeat the baseline test for each day of testing and compare to the initially defined baseline runs. Determine overall non-repeatability in baseline operation and determine typical variations in control, performance and emissions parameter values.

3.0 Exhaust Sampling System Description

Specific protocols for sample collection will be submitted to the IC Engine Work Group for review and approval prior to testing. In general, the samples will be collected as described below.

3.1 Criteria Pollutant Reference Method System

Reference Method (RM) trailers will draw an exhaust sample via a probe installed downstream of the turbochargers if so equipped. The conditioned sample will then pass through a common manifold to criteria pollutant analyzers. Each analyzer will output a signal to a Data Acquisition System (RMDAQ) which will correct the data for drift and calculate mass and brake-specific emissions rates. The RMDAQ also will continuously hand the emissions analyzer data off to the database data acquisition system (DBDAQ).

3.2 HAPs FTIR System

HAPs FTIR trailers will draw exhaust from a train probe mounted adjacent to the RM probe. The sample is passed through the FTIR. The FTIR DAQ will perform the necessary Fourier analyses and then determine and display/archive/print the resultant emissions. The FTIR DAQ also will continuously hand the emissions data off to the DBDAQ.

4.0 Data Collection

Specific protocols for collecting engine parameter data, emissions data, and specifications for the data acquisition systems will be submitted to the IC Engine Work Group for review and approval prior to testing. Fuel analysis will be conducted for all emissions tests. In general, engine parameter data must meet the minimum requirements specified below.

4.1 Hardware Description

Must be able to pull all engine operating parameters as well as emissions (criteria and HAPs) into a common database (DBDAQ). May or may not be separate data acquisition system.

4.2 Emissions Data

Data on criteria and HAP pollutants must be supplied to a central data acquisition system.

4.3 Engine Operating and Performance Parameters

The minimum data that will be transmitted to the DBDAQ includes:

Engine Speed Engine Torque or Load Spark or Injection Timing Intake Manifold Pressure (IMP) Intake Manifold Temperature (IMT) Fuel Flow Rate Air Flow Rate Exhaust Manifold Temperature (upstream of TC if so equipped) Jacket Water Temperature (JWT)

Other data may include:

Intercooler Water Temperature (IWT) if so equipped Inlet Air Temperature (ambient) Inlet Air Pressure (ambient barometer) Ambient Humidity **Exhaust Manifold Pressure Turbocharger Speed**

In addition, the following data will be recorded where available and/or applicable:

Average peak combustion pressure Location of peak combustion pressure Standard deviation of the peak combustion pressure

Individual cylinder exhaust temperatures

4.4 Data Reduction

During actual testing, the DBDAQ will scan all inputs at a rate of 1 Hz and perform all relevant calculations continuously, including:

Fuel Flow Exhaust Flow (O_2 Balance) Exhaust Flow (C Balance) Air Flow Air/Fuel Ratio F/A Equivalence Ratio Brake Specific Fuel Consumption (BSFC) Emissions Mass Rates (NO_x , CO, THC & HAPs) Brake Specific Emissions Rate (NO_x , CO, THC, & HAPs)

Upon successful completion of each test run, the test director will archive the data on the DBDAQ hard drive, import the data into a preliminary Test Condition Summary Data Sheet and print a preliminary copy of the data for review and comparison with other test runs.

APPENDIX D:Response to Comments Received on Pollutant Lists

1.0 Lists of Pollutants Presented at the July Coordinating Committee Meeting

The lists of the pollutants proposed by the RICE Work Group for the purpose of emissions testing are provided below. The RICE Work Group has not yet determined which pollutants may be regulated for RICE under ICCR.

Diesel Fuel (for emissions testing only)

- 1. 1,3-Butadiene
- 2. Acetaldehyde
- 3. Acrolein
- 4. Benzene
- 5. Beryllium
- 6. Cadmium
- 7. Chromium
- 8. Ethylbenzene
- 9. Formaldehyde
- 10. Hexane
- 11. Lead
- 12. Manganese
- 13. Mercury
- 14. Naphthalene
- 15. Nickel
- 16. POMs (PAHs)
- 17. Selenium
- 18. Toluene
- 19. Xylene

Digester Gas (for emissions testing only)

- 1. 1,4-Dichlorobenzene(p)
- 2. Acetaldehyde
- 3. Acrolein
- 4. Benzene
- 5. Ethylbenzene
- 6. Formaldehyde
- 7. Methylene Chloride
- 8. Styrene
- 9. Toluene
- 10. Vinyl Chloride

11. Xylene

Landfill Gas (for emissions testing only)

- 1. Acetaldehyde
- 2. Acrolein
- 3. Benzene
- 4. Carbon Tetrachloride
- 5. Chloroform
- 6. Ethylbenzene
- 7. Formaldehyde
- 8. Methyl Chloroform (1,1,1-Trichloroethane)
- 9. Tetrachloroethylene (Perchloroethylene)
- 10. Toluene
- 11. Trichloroethylene
- 12. Vinyl Chloride
- 13. Xylene

Natural Gas (for emissions testing only)

- 1. 1,1,2,2-Tetrachloroethane
- 2. 1,3-Butadiene
- 3. Acetaldehyde
- 4. Acrolein
- 5. Benzene
- 6. Chlorobenzene
- 7. Ethylbenzene
- 8. Ethyl Chloride (Chloroethane)
- 9. Formaldehyde
- 10. Methylene Chloride
- 11. Naphthalene
- 12. POMs (PAHs)
- 13. Toluene
- 14. Xylene

Propane (for emissions testing only)

- 1. Acetaldehyde
- 2. Acrolein
- 3. Benzene

- 4. Ethylbenzene
- 5. Formaldehyde
- 6. Naphthalene
- 7. Toluene
- 8. Xylene

2.0 Request For Input On Pollutants To Be Tested

In response to comments received at the July Coordinating Committee meeting, the Reciprocating Internal Combustion Engine (RICE) Work Group accepted recommendations for additional pollutants which should be included in plans for future emissions testing of internal combustion engines under ICCR.

Comments Received on Pollutants To Be Tested 3.0 and Work Group Responses

Seven comments were received from members of ICCR outside the RICE Work Group in response to the Work Group's request for input on the pollutant lists. The comments and the Work Group's responses are provided below.

COMMENT #1

From: Richard Van Frank, INTERNET:vanfrank@iquest.net

Date: 8/2/97 9:35 PM

RE: Hg-landfill gas

Sender: vanfrank@iquest.net

This is one reference to Hg in landfill gas; one that the EPA should have known about. There are many other references to this in the literature.

Determination of Landfill Gas Composition and Pollutant Emission Rates at Fresh Kills Landfill-Project Data (on diskette)

Summary:

Air emissions of landfill gas pollutants at Fresh Kills Landfill, located in Staten Island, NY, were estimated based on three weeks of sampling of flow, concentration, and flux at passive vents, gas extraction wells, gas collection plant headers, and the landfill surface conducted by Radian Corporation in 1995. Emission rates were estimated for 202 pollutants, including hydrogen sulfide, mercury vapor, speciated volatile organic compounds, methane, and carbon dioxide. Results indicate that large amounts of mercury enter the methane recovery plant. Emission factors based on the results are presented.

Additional information:

Format: Diskette. The datafile is on one 3 ½ inch DOS diskette, 1.44M high density.

This product contains text only. Customers must provide their own search and retrieval software.

Work Group Response

Mercury was not added to the list of pollutants to be tested. No engines using landfill gas will be tested as a part of this test plan. Also, review of the data cited revealed extremely low mercury emissions from the entire landfill, 2.3 pounds per year.

The Fresh Kills is the largest landfill in the US, over 3,000 acres, located on Staten Island. The landfill processes 13,000 tons / day. Initial testing of the landfill indicated that mercury emissions were .00545 g/sec. This corresponds to 378 pounds/yr. The mercury measurements were performed using a portable analyzer rather than the standard EPA reference method. The results were noted as being particularly high, which raised more questions about the testing methodology. A follow-on study was commissioned to examine the mercury emissions in more depth, using EPA reference methods. The follow-up test showed much lower mercury emissions, a total of 2.3 lb/yr from the entire landfill.

COMMENT #2

Date: August 1, 1997

From: Tom McGrath, Energy and Environmental Research Corporation

I attended the ICCR Coordinating Committee Meting in Long Beach, CA on July 23 including the

RICE work group presentation of "Pollutants Identified for Emissions Testing Under ICCR." I also attended the ICCR Testing and Monitoring Protocol work group meeting on July 25 and expressed some comments regarding the RICE work group presentation. The ICCR Testing and Monitoring Protocol work group suggested I send my comments directly to you. These comments are:

The proposed lists of HAPs to be included in Test Plans for IC engines firing the fuels natural gas and diesel are well supported by the existing HAPs emissions data. My understanding from the Coordinating Committee meeting is that someone is to investigate which HAPs may be formed under combustion conditions based on the composition of inlet streams and combustion chemistry. You may want to consult this "potential HAPs" list prior to finalizing the HAPs lists for natural gas and diesel fuel (and all other fuels).

This comment references the Table from the presentation entitled "Pollutants Reported as "Detects"." Seven HAPs were measured during the single propane test reported and all seven HAPs were detected. Nine HAPs were measured during the single landfill gas test reported and all nine HAPs were detected. These data suggest other HAPs, which were not measured, may be present in the exhaust of IC engines firing these fuels. Propane and landfill gas are more complex fuels than natural gas. It therefore follows that HAPs emissions from IC engines firing propane and landfill gas will be at least as great as HAPs emissions from IC engines firing natural gas. This suggests that the propane and landfill gas HAPs list should include all HAPs detected in the exhausts of IC engines firing natural gas.

- It is expected that landfill gases contain organo-chlorines from the breakdown of municipal waste. Emissions of chlorinated HAPs from landfill gas combustion in IC engines are therefore possible either as uncombusted landfill gas constituents or as products of incomplete combustion. This suggests the landfill gas HAPs list should include the chlorinated HAPs species that have been detected in other tests and/or listed in the "potential HAPs" list referenced in Comment 1.
- 1,4-Dichlorobenzene(p) was measured in the exhaust of IC engines firing digester gas. Measurements of chlorobenzene were not made. The formation of chlorobenzene only requires the extraction of one chlorine atom from 1,4-Dichlorobenzene(p). The presence of 1,4-Dichlorobenzene(p) suggests chlorobenzene should be measured during future tests.

Naphthalene was detected in the exhaust of IC engines firing propane and is included in the Table from the presentation titled "Proposed Pollutants for Emissions Tests Under ICCR".

Naphthalene is the lightest polycyclic aromatic hydrocarbon (PAH) and is likely a building

block for heavier PAH. This suggests PAH measurements should be included in the IC engines tests firing propane.

Please note that the additional target HAPs suggested in this correspondence do not necessarily require additional test methods and testing costs. Most of the additional HAPs suggested in this correspondence can be measured by the methods that will be required to measure the HAPs listed in the Table from the presentation titled "Proposed Pollutants for Emissions Tests Under ICCR".

Please contact me at (714) 552-1803 if you have questions or require clarification of these comments.

Work Group Response

The list of "potential HAPs" developed by the Testing and Monitoring Protocol Work Group has been compared to the lists of pollutants for diesel fuel and natural gas. If the Coordinating Committee prepares another list of potential HAPs, the RICE Work Group will compare the lists of pollutants to be tested to that list, to determine if any pollutants should be added to the testing program.

The list of HAPs for natural gas has been compared with the lists for other fuels.

For digester gas, 1,3-butadiene, naphthalene, and PAHs are the only pollutants on the natural gas list (save the chlorinated compounds, which were reported for natural gas apparently as a result of field contamination of the samples, see Work Group Response to Comment #6) that are not on the digester gas list. 1,3-butadiene was tested for RICE using digester gas multiple times (see ICCR Emissions Database for RICE) and was never detected. If no 1,3-butadiene is present, it is reasonable to assume there is no naphthalene or PAHs present.

For diesel, all the HAPs included on the natural gas list are on the diesel fuel list, save the chlorinated compounds. Since the chlorinated compounds apparently were reported for natural gas as a result of field contamination of the samples (see Work Group Response to Comment #6), no additional pollutants have been added for diesel fuel.

For landfill gas, 1,3-butadiene, naphthalene, and PAHs are the only pollutants on the natural gas list (save the chlorinated compounds, see Work Group Response to Comment #6) that are not on the landfill list. There are no tests for these compounds in the ICCR Emissions Database for RICE. These compounds will be

added to the pollutant list for landfill gas.

For propane, 1,3-butadiene and PAHs are the only pollutants on the natural gas list (save the chlorinated compounds, see Work Group Response to Comment #6) that are not on the propane list. Since Naphthalene was detected for propane, it is reasonable to assume that 1,3-butadiene and PAHs may be present. These compounds will be added to the pollutant list for propane.

The chlorinated compounds reported in the ICCR Emissions Database for fuels other than landfill gas are 1,1,2,2-tetrachloroethane, chlorobenzene, ethyl chloride, methylene chloride, 1,4-dichlorobenzene(p), and vinyl chloride. These compounds will be added to the pollutant list for landfill gas.

1. RICE Work Group stakeholders familiar with digester gas indicate that chlorobenzene has been tested for RICE using digester gas and is reported 9 times out of 10 as a non-detect. Chlorobenzene will not be added to the pollutant list for digester gas.

Since Naphthalene was detected, it is reasonable to assume PAHs may be present. PAHs will be added to the pollutant list for propane.

The Work Group agrees that the additional HAPs can be quantified with the test methods proposed under this Test Plan, for little, if any, additional cost.

COMMENT #3

Date: Thu, 21 Aug 1997 13:01:08 -0500

From: "William O'Sullivan" < WOSULLIV@dep.state.nj.us

As discussed at the last Coordinating Committee meeting, testing should include the following:

1. CO, particulates and NOx - These criteria pollutants are important in order to better correlate toxic emissions with combustion conditions. Sometimes high organic HAPS are simply the result of poor combustion, which can be best recognized from high CO levels. Correlation of low HAPs with low CO may lead to use of CO limits and monitoring as MACT for organic HAPs. NOx is needed to weigh the environmental consequences of combustion conditions that may increase NOx, but decrease HAPs and CO. Particulates are needed for the same reason; that is we may need to weigh NOx increases against CO, HAP and particulate decreases in some cases. Also, the coordinating committee may want to recommend NOx, particulate,

and CO control measures; along with HAP control measures.

2. The fuels should be tested for at least the inorganic HAPs which are likely to be in these fuels, including mercury. Where the inorganic HAP is likely not to be caught by an air pollution control device, then fuel testing for the HAP is sufficient. Mercury will fall into this category for most units. Some of the stack testing for the other inorganic metals might be deleted and replaced with fuel testing results where it is expected that most of the metal will be emitted because there is no particulate control device on the unit.

Work Group Response

Criteria pollutants, including CO, PM, NOx, and THC will be measured simultaneously with the HAP measurements.

Fuel testing for metals in diesel fuel has been added to the Test Plan, in lieu of stack measurements for metals.

"Jeffrey.Shumaker@ipaper.com [SMTP:Jeffrey.Shumaker on 08/20/97 12:02:00 PM

To: Sam Clowney

cc:

Subject: Re: Request for Input on Pollutants to be Tested for RICE

I submit for your consideration the idea of sampling for methanol from digester gas combustion. I'm not sure what materials are digested in the units fueling IC engines, but methanol is clearly an issue in the digestion of wood to produce paper fiber and I presume it could be an issue with other cellulose-containing biomass. For example, methanol is the primary indicator HAP in the MACT for pulp mills.

I am not suggesting that methanol is a dangerous HAP. In fact, we have a petition pending at EPA to remove methanol from the HAP list altogether. However, if it is present in quantity, it could be an indicator of proper combustion.

It may well be that I'm off-base given the digestion process(es) you are working with and I'm not suggesting that I or the industry I represent feels testing of methanol is important or even known to be warranted. I simply wanted to bring this potential issue to your attention.

Work Group Response

RICE Work Group Stakeholders familiar with RICE using digester gas reviewed this issue. Orange County tested for methanol in 1995 and no methanol was detected in any test. Methanol will not be added to the pollutant list for digester gas.

COMMENT #5

Date: Wed, 27 Aug 1997 15:58:18 -0400 From: Michael Wax <mwax@icac.com

Reply-To: mwax@icac.com

Organization: Institute of Clean Air Companies

To: jsnyder@alpha-gamma.com Subject: Your Message of August 20

Based on elementary combustion chemistry, any compounds found in the exhaust of natural gas-fired engines also is very likely to be found in the exhaust of digester gas-, landfill gas-, and propane-fired engines. Therefore, I suggest adding all of the natural gas compounds listed, with the possible exception of the chlorinated compounds, to the other lists.

Work Group Response

The Work Group reviewed the list of pollutants reported for natural gas, save the chlorinated compounds (see Work Group Response to Comment #6). The results of this comparison are summarized under Work Group Response to Comment #2.

COMMENT #6

FROM: Michael J. Atherton, Columbia Gas

SUBJECT: RICE Work Group, Request for Additional Pollutants for Emissions Testing

This Group identified 14 hazardous air pollutants that should be included in plans for future testing of natural gas reciprocating engines. The list includes 4 chlorinated hydrocarbons (1,1,2,2-Tetrachloroethane, chlorobenzene, ethyl chloride and methylene chloride). The chlorination of alkanes requires chlorine (Cl_2) and a temperature at 250 - 400**E** C; the chlorination of benzene requires Cl_2 and $FeCl_3$; the chlorination of alkenes requires the presence of Cl_2 and the reaction is usually carried out in an inert solvent such as carbon tetrachloride; alkenes can also be chlorinated using hydrochloric acid, the first step being the transfer of hydrogen in the HCl to the alkene molecule. Since natural gas does not contain Cl_2 or HCl, these chlorinated compounds will not be formed during combustion and there is no reason to include these compounds in the list. These reactions are discussed in any introductory course in organic chemistry.

Small quantities of chloride ion (Cl^-) from produced water may be entrained in the natural gas but cannot result in the production of chlorinated hydrocarbons. The mechanisms require either Cl_2 or HCl.

Work Group Response:

The RICE Work Group requested that Dr. Laura Kinner of Emissions Monitoring, Incorporated, review the two test reports in the ICCR Emissions Database that report quantities of chlorinated compounds for natural gas sources. Dr. Kinner's findings, provided below, indicate that there is evidence of field contamination of the exhaust samples. The Work Group concludes that the compounds were not present in the exhaust, but were introduced by contamination during the sample collection process. Therefore, the chlorinated compounds have been removed from the pollutant list for natural gas.

Summary of Dr. Kinner's findings:

Chlorinated volatile organic compounds were reported in natural gas-fired reciprocating engine effluent at concentration levels in the low parts per billion. The chlorine source for the thermal formation of these compounds is unknown; however, the fuel source is not suspected by industry representatives to contribute chlorine for these reactions.

The test methods used during the two subject field tests at natural gas-fired reciprocating engines were SW846 - 0030 (VOST) and Method TO - 14. The VOST method employs a combination of Tenax and Tenax and activated charcoal adsorbent traps as sample collection media. Analysis is accomplished by thermal desorption of the traps onto a separate Tenax trap, followed by desorption onto a

GC column. Detection of the compounds is accomplished by a mass spectrometer. Method TO - 14 employs an evacuated SUMMA canister to withdraw sample gas from the source. The gas sample is analyzed by adsorption onto a Tenax trap or cryogenically cooled trap, followed by desorption onto a GC column. Detection of the compounds is accomplished by a mass spectrometer. Because a mass spectrometer is a specific detector, it is unlikely that the chlorinated volatile organic compounds that were detected were misidentified.

Contamination of various sample collection and analysis media by volatile organic compounds is encountered frequently in practice, and is difficult and sometimes impossible to eliminate. Compounds such as toluene, methylene chloride, carbon tetrachloride and trichloroethane are common laboratory solvents that frequently are detected in method blank samples because of their ubiquitous use as laboratory and field sample recovery solvents. It is postulated that the source of the volatile chlorinated compounds detected in the natural gas-fired effluent is derived from low concentration level contamination of the sample collection and analysis media by laboratory solvents, or possibly carryover from other testing projects.

Examination of both subject reports reveals the following information. One report contains data indicating low concentration levels of chlorobenzene, chloroethane, 1,1-dichloroethane and tetrachloroethane collected by the VOST method. It is unclear from the report whether any chlorinated volatile organic compounds were detected in the field and laboratory blank samples during this testing program. Therefore, the level of potential field or laboratory contamination can not be assessed. The second report employing Method TO - 14 contains data for numerous organic compounds collected from five natural gas-fired reciprocating engines. Almost every TO - 14 field sample reports data for chlorinated compounds, specifically methylene chloride and trichlorethane. Data from laboratory blank samples show no evidence of contamination; however, the field blank samples contained substantial levels of methylene chloride and trichlorethane relative to those levels reported in actual effluent samples. The field blank data are limited to only two samples collected during the testing project duration; however they support the hypothesis that the natural gas-fired effluent is not the source of chlorinated volatile organic compounds.

COMMENT #7

FROM: Lee Gilmer

Subject: Engine Testing HAPs list

Comment A:

We have some questions/concerns regarding the subject list. Specifically:

- * Diesel Fuel We question the inclusion of beryllium, cadmium, and chromium. Is there actual data (not below detection limit values) that suggest these compounds are present in diesel exhaust? If not, what is the basis for including them? If so, is it reasonable to expect these compounds to really be present?
- * Natural gas We question the inclusion of 1,1,2,2-tetrachlorethane, chlorobenzene, ethyl chloride (chloroethane), methylene chloride, and 1,3-butadiene. Same questions as above. Also, is there data that conclusively attributes any of these compounds to transmission gas as opposed to raw gas? Can you explain why some of the lighter organics even if present in the fuel wouldn't be destroyed in the combustion process?

Comment B: I just happened to notice a bottle of methylene chloride sitting on a table in one of our labs where GC analyses are performed. This jogged my memory that various solvents including methylene chloride are used in analytical labs. I'm pretty sure the only way methylene chloride can be measured in engine exhaust samples is to use an analytical device which just may happen to use some laboratory equipment that may have been exposed to methylene chloride. I have confirmed this with members of the ICCR Testing and Monitoring Workgroup. I believe it would be a travesty if somehow/someway ICCR regulations were developed on HAPs that showed up in testing reports due to such testing artifacts.

Work Group Response

Comment A: Fuel testing for metals has been adopted as a part of the RICE Test Plan in lieu of stack testing for metals (see Work Group Response to Comment #3). The chlorinated compounds have been removed from the list of pollutants to be tested for natural gas as a result of Dr. Kinner's finding that the chlorine was introduced as a contaminant during the sample

collection process in the field (see Work Group Response to Comment #6).

Comment B: Methylene chloride is used commonly in laboratories and often can be a contaminant. Based on Dr. Kinner's review of the test reports, there is evidence that the chlorine reported for natural gas-fired engines was introduced as a contaminant during the sample collection process in the field (see Work Group Response to Comment #6).

4.0 Revised Lists of Pollutants to be Tested

The revised lists of the HAP pollutants to be tested are provided below. Please note that these lists were developed for the purpose of emissions testing only. The RICE Work Group has not yet determined which pollutants may be regulated for RICE under ICCR.

Diesel Fuel (for emissions testing only)

- 1. 1,3-Butadiene
- 2. Acetaldehyde
- 3. Acrolein
- 4. Benzene
- 5. Beryllium
- 6. Cadmium
- 7. Chromium
- 8. Ethylbenzene
- 9. Formaldehyde
- 10. Hexane
- 11. Lead
- 12. Manganese
- 13. Mercury
- 14. Naphthalene
- 15. Nickel
- 16. POMs (PAHs)
- 17. Selenium
- 18. Toluene
- 19. Xylene

Digester Gas (for emissions testing only)

- 1. 1,4-Dichlorobenzene(p)
- 2. Acetaldehyde
- 3. Acrolein

- 4. Benzene
- 5. Ethylbenzene
- 6. Formaldehyde
- 7. Methylene Chloride
- 8. Styrene
- 9. Toluene
- 10. Vinyl Chloride
- 11. Xylene

Landfill Gas (for emissions testing only)

- 1. Acetaldehyde
- 2. Acrolein
- 3. Benzene
- 4. Carbon Tetrachloride
- 5. Chloroform
- 6. Ethylbenzene
- 7. Formaldehyde
- 8. Methyl Chloroform (1,1,1-Trichloroethane)
- 9. Tetrachloroethylene (Perchloroethylene)
- 10. Toluene
- 11. Trichloroethylene
- 12. Vinyl Chloride
- 13. Xylene
- 14. 1,3-Butadiene (new)
- 15. Naphthalene (new)
- 16. POMs (PAHs) (new)
- 17. 1,2,3,3-Tetrachloroethane (new)
- 18. Chlorobenzene (new)
- 19. Ethyl Chloride (new)
- 20. Methylene Chloride (new)
- 21. 1,4-Dichlorobenzene(p) (new)
- 22. Vinyl Chloride (new)

Natural Gas (for emissions testing only)

- 1. 1,3-Butadiene
- 2. Acetaldehyde
- 3. Acrolein

- 4. Benzene
- 5. Ethylbenzene
- 6. Formaldehyde
- 7. Naphthalene
- 8. POMs (PAHs)
- 9. Toluene
- 10. Xylene

Propane (for emissions testing only)

- 1. Acetaldehyde
- 2. Acrolein
- 3. Benzene
- 4. Ethylbenzene
- 5. Formaldehyde
- 6. Naphthalene
- 7. Toluene
- 8. Xylene
- 9. 1,3-butadiene (new)
- 10. POMs (PAHs) (new)

APPENDIX E: Estimated Costs to Conduct RICE Emissions Testing

The RICE Work Group requested assistance from the Testing and Monitoring Protocol Work Group to estimate the costs to perform the emissions testing outlined in this Test Plan. The Testing and Monitoring Work Group estimated that the four emissions tests proposed, data analysis, and data reporting would cost **\$610,000**, assuming that the test sites are located in "reasonably accessible locations."

ATTACHMENT V TEST PLAN PRESENTATION

Test Plan for Reciprocating Internal Combustion Engines

presented to:

ICCR Coordinating Committee Houston, Texas

presented by:

Sam Clowney, Tennessee Gas Pipeline, on behalf of the Reciprocating Internal Combustion Engine (RICE) Work Group

November 18-19, 1997

Topics

- Purpose of Briefing
- Context for Plan Development
- Test Plan Development Process
- Content of Test Plan
- Cost and Schedule

Purpose of Briefing

- Provide the Coordinating Committee background on the need for RICE emissions testing
- Inform the Coordinating Committee about the process to develop the RICE Test Plan and the contents of the Test Plan
- Provide the Coordinating Committee an opportunity to provide guidance relative to coordinating this testing with other Work Groups
- Inform the Coordinating Committee about the costs and schedule to conduct this Test Plan

Context for Plan Development

- Coordinating Committee directed Work Groups to identify testing needs during March 1997 meeting
- EPA stressed that very limited funds would be available for HAPs emissions testing
- Unexplained variability in emissions data included in ICCR Emissions Database for reciprocating internal combustion engines
 - emission factors for formaldehyde emissions from natural gas-fired engines over 6 orders of magnitude
- Multiple emissions data gaps identified

Process to Develop Test Plan

(1 of 4)

- Emissions Subgroup assigned task to identify testing needs for RICE Work Group
 - 19 members, all stakeholders represented
 - » Industry, local governments, engine manufacturers, state representatives, academics, and EPA
- First step: Identify pollutants to be tested
 - Presented to Coordinating Committee in July, comments on pollutants accepted until September 5
- Second step: Identify test methods to use

Process to Develop Test Plan

- Third Step: Address Engine Considerations:
 - Operating Conditions
 - » Based on industry experience with criteria pollutants, such as NOx, believe operating conditions can affect HAP emissions and efficiency of controls
 - Need to conduct testing over full operating range
 - Need person with knowledge of engine operations on site to establish condition of engine
 - Need to collect adequate operating parameter data to relate operating conditions and emissions

Process to Develop Test Plan

(3 of 4)

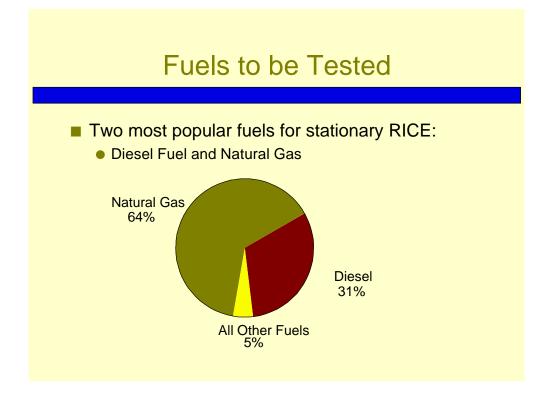
- Engine Considerations (cont.)
 - Diversity of Existing Engine Population
 - » Over 3,000 possible combinations
 - Operating cycle (spark ignition or compression ignition)
 - Fuel
 - Scavenging cycle (2-stroke or 4-stroke)
 - Air-to-fuel ratio (rich or lean)
 - Make and model
 - Size
 - Driven equipment and application

Process to Develop Test Plan

- Plan developed over past 8 months
 - Numerous conference calls to develop content
 - Experts provided input on key components:
 - » Testing and Monitoring Protocol Work Group
 - » Engine and other testing experts
 - Components of plan reviewed at May, September, & October Work Group meetings
 - Multiple drafts of plan reviewed by Work Group
- Work Group consensus on final plan achieved on October 30, 1997

Content of Test Plan

- Four Emissions Tests Proposed
- Components of Tests:
 - Fuels, Engines, and Emission Controls to be Tested
 - Matrix of Operating Conditions
 - Pollutants to be Tested
 - Test Methods to Quantify Pollutants



Engines to be Tested

- Diesel (CI)
 - Caterpillar 3500
- Natural Gas (SI, 2- and 4-stroke, rich and lean)
 - 2-stroke:
 - » Clark TLA, turbocharged
 - 4-stroke, lean-burn
 - » Waukesha 7042 GL, turbocharged
 - 4-stroke, rich-burn
 - » Ingersoll Rand KVG, naturally aspirated

Controls to be Tested

- Focus on devices identified as possible maximum achievable control technology (MACT)
 - Oxidation catalysts for lean-burn engines
 - Non-selective catalytic reduction (NSCR) three-way catalysts for rich-burn engines

Matrix of Operating Conditions

- In order to test entire operating range, Work Group developed16-point test matrix
- Four corners of torque/speed envelope (runs 1-4)
- Air-to-fuel ratio sensitivity (runs 1, 5-6)
- High speed and low load (run 7)
- Low speed and high load (run 8)
- Air manifold temperature sensitivity (runs 1, 9-10)
- Jacket water temperature sensitivity (runs 13-14)



Pollutants to be Tested

- Both criteria pollutants and HAPs to be tested before and after pollution control devices
- Criteria Pollutants:
 - carbon monoxide (CO), nitrogen oxides (NOx), total hydrocarbons (THC), particulate matter (PM) (diesel only)
- HAPs:
 - BTEX (benzene, toluene, ethylbenzene and xylene)
 - Aldehydes (formaldehyde, acetaldehyde acrolein)
 - Naphthalene, 1_v3-butadiene, PAHs
 - n-Hexane (diesel only)
 - metals (diesel only)

Test Methods (1 of 2)

- Test methods selected that will provide direct measurement and reporting of pollutant concentrations on-site, whenever possible
- No EPA-approved method to measure PM from stationary engines -- only EPA-approved method for RICE is ISO Method 8178, which was developed for non-road mobile engines
- Testing to be conducted to achieve lowest practical detection limits for all compounds

Test Methods (2 of 2)

Test Method	Sample Time	Pollutants	Achievable Dete
Direct Interface COMS	10 minutes	BTEX 1,3-Butadiene	50 ppb 75 ppb
33.12		Hexane	75 ppb
FTIR V	10 minutes - 8	BTEX 1,3-Butadiene Hexane Formaldehyde Acetaldehyde Acetaldehyde	>3pm >3ppm >10ppm 100ppb 100ppb

Costs and Schedule

Cost to Conduct Test Plan:

\$610,000

Schedule:

• November 1997 Work Group to submit

Plan to EPA and request funding

• Fall 1997 Work Group to identify test sites

• Spring 1998 EPA Contractor to conduct testing

ATTACHMENT VI

PRELIMINARY MACT FLOOR PRESENTATION

Preliminary MACT Floor

Population Subgroup Wayne A. Hamilton

RICE Work Group 10/30/97 Presentation

Overview

- Summary
 - » Engine Type
 - » Emission Controls
- Preliminary MACT Floor Procedure
 - » Information Source
 - » Database Refinement
 - » Statistics
 - » Preliminary MACT Floor

Summary

- SIGF: Natural Gas 2-Stroke Lean Burn
 - » Conclusion: No Controls At MACT Floor
 - » 99% No equipment
 - » 1% Nonsense controls
 - » Total: 853

Summary

- SIGF: Natural Gas 4-Stroke Lean Burn
 - » Conclusion: No Controls At MACT Floor?
 - » 90% No equipment?
 - » 8% Catalytic Reduction
 - » Total: 658
- SIGF: Natural Gas 4-Stroke Rich Burn
 - » Conclusion: Controls At MACT Floor
 - » 79% No equipment
 - » 18% Catalytic Reduction
 - » Total: 878

Challenges

- Data
 - » New Mexico Over-Represented
 - » Industry Over-Represented
 - » Horsepower
- Controls
 - » HAPs Effectiveness?
- Solutions
 - » Compare Information
 - » Control Subgroup

Information Source

- Engines: 28,000+
- Source: EPA ICCR Version 2 Database in Access 2.0
- Number of States/Territories: 55

Database Refinement

- Majority of Work
- Alpha-Gamma
 - » Write-up of database refinement activities to WG by E-mail and TTN
- Obtain More Information
 - » Make and Model Information
 - » Verify questionable information

Database Refinement: Nonsense Control Devices

- Incorrect Control Devices: 248 Records or 1%
- Control Devices Designation
- Verified Nonsense Control Devices

Database Refinement: Blank Control Field

- Blanks = "No Equipment"
 - » 22,597 records were changed (64%)
- Verified Blank Control Devices with Eight States (68% of population)

» Texas (18%) blanks = no control devices

» California (14%) not a required field, therefore not reliable

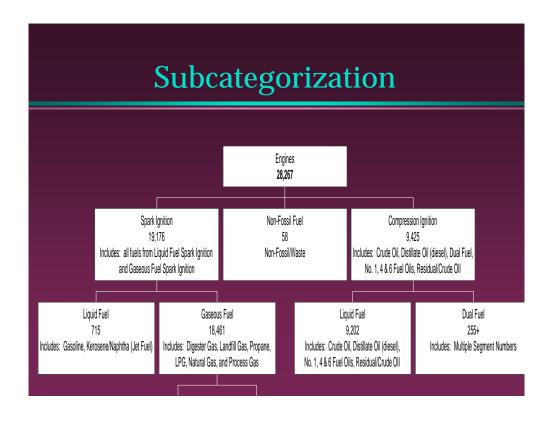
» Louisiana (10%) blanks = no control devices
 » New Mexico (7%) blanks = no control devices
 » Colorado (5%) blanks = no control devices
 » Oklahoma (5%) blanks = no control devices

» New Jersey (4%) blanks = no control devices

» Michigan (4%) blanks = no control devices (unconfirmed)

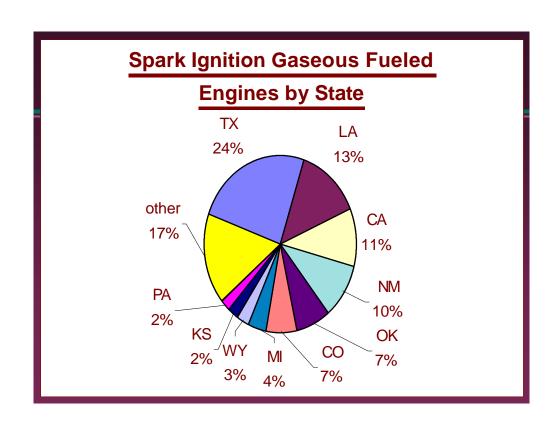
Database Refinement: Calculations

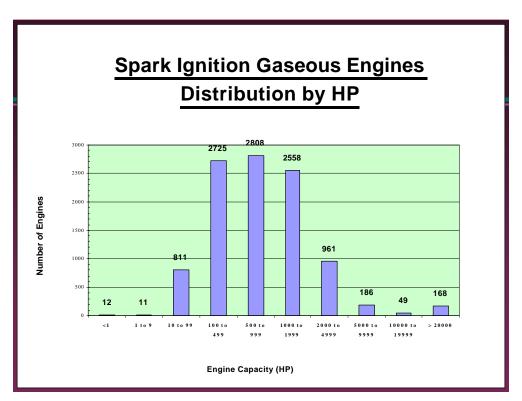
- Efficiency
 - » Convert to horsepower
 - » WG members recommended
 - 34% for lean burn
 - 32% for rich burn



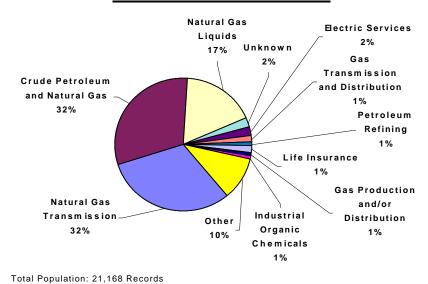
Engine Statistics

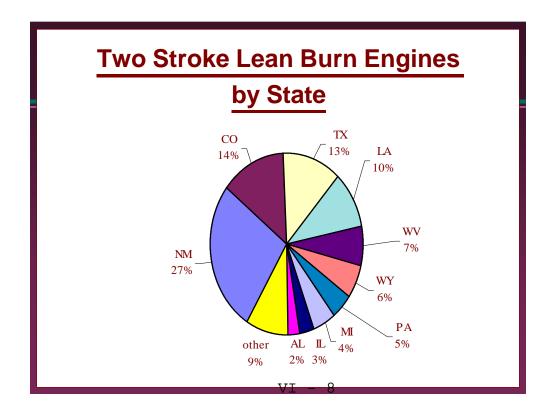
- Engines: Gas, 2-Stroke, 4 Stroke, Liquid
 - » Engine Distribution by State
 - » Engine Distribution by Horsepower
 - » Engine Distribution by Industry
- Data Limitation

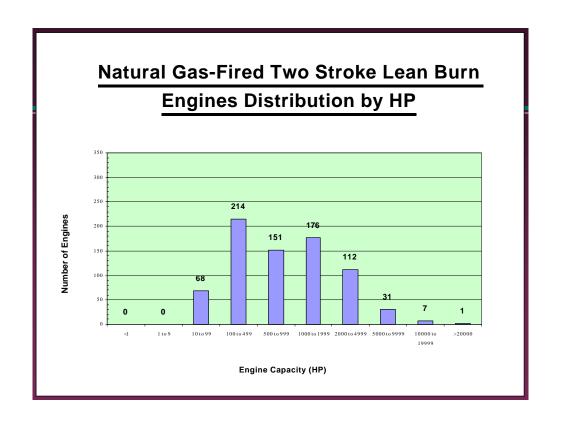


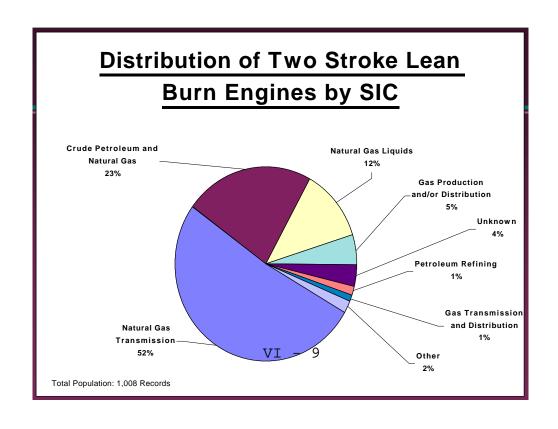


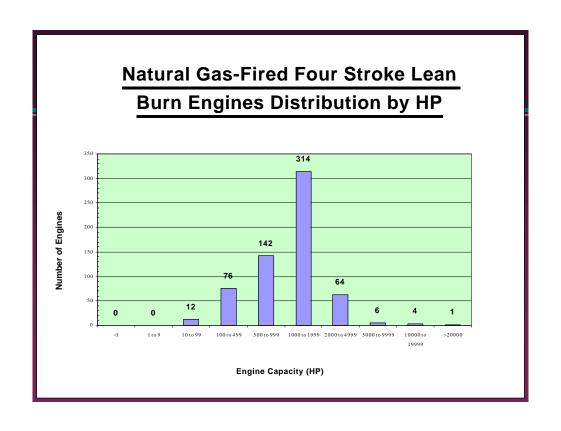
Distribution of Spark Ignition Gaseous Fueled Engines by SIC

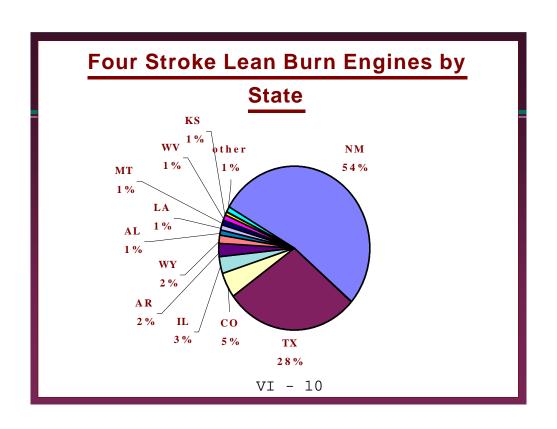


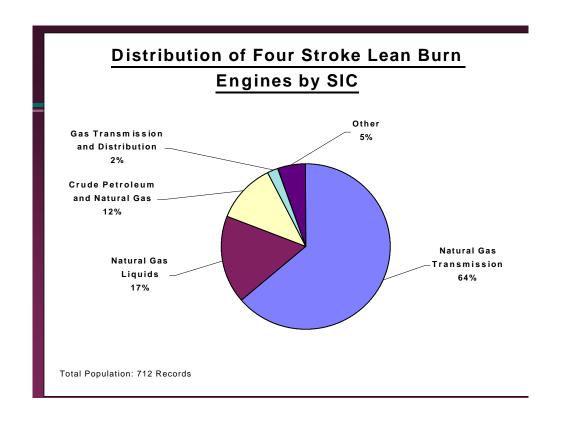


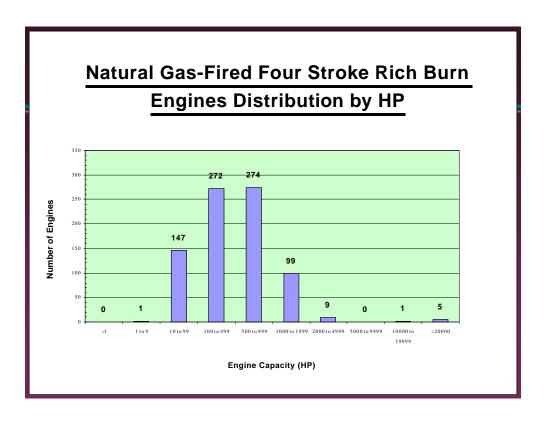


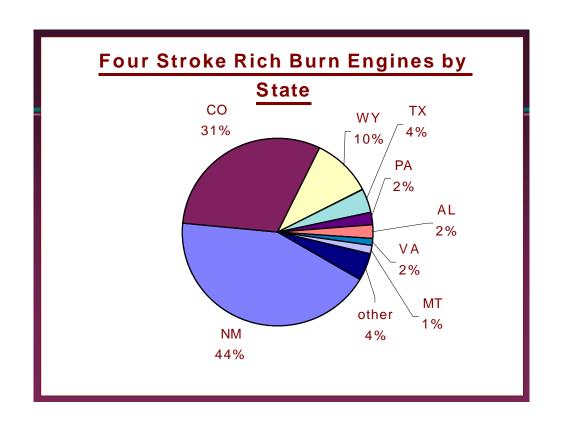


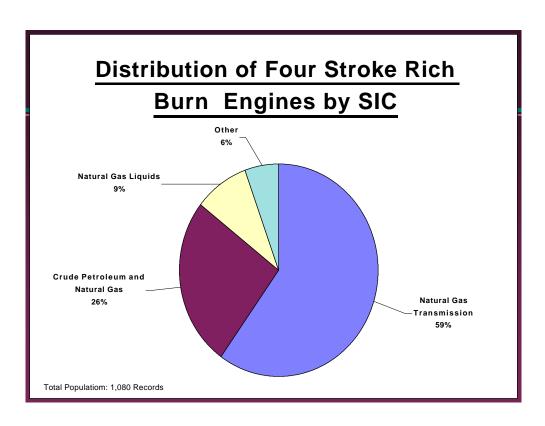












Action Items

- API database November 11, 1997
 - » Compare Results
 - » Industry Specific
- Power Systems Research
 - » Non-Road Vs Stationary
 - » No Control Devices

Recommendation

- Coordinating Committee Update
 - » Preliminary MACT Floor Defined
- Coordinating Committee Presentation After:
 - » Lean Burn Validation
 - » API Data
 - » Power Systems
 - » When: Winter 1998

Summary

- Two Stroke: Preliminary MACT Floor
 - » Conclusion: No Controls At MACT Floor
 - » 99% No Controls

Summary

- Four Stroke: Preliminary MACT Floor
 - » Rich Burn: 78% No Controls
 - Conclusion: Controls At MACT Floor
 - » Lean Burn: 90% No Controls
 - Conclusion: No Controls At MACT Floor? $^{
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